

2.2V, 50MHz, Low-Noise, Single-Supply Rail-to-Rail OPERATIONAL AMPLIFIERS

FEATURES

- **RAIL-TO-RAIL INPUT WITHOUT CROSSOVER**
- **2.2V OPERATION**
- **LOW OFFSET: 200**µ**V**
- **WIDE BANDWIDTH: 50MHz**
- **CMRR: 100dB (min)**
- **HIGH SLEW RATE: 25V/**µ**s**
- **LOW NOISE: 4.5nV/Hz**
- **LOW THD+NOISE: 0.0006%**
- **QUIESCENT CURRENT: 5mA (max)**
- **microPACKAGE: SOT23-5**

APPLICATIONS

- **SIGNAL CONDITIONING**
- **DATA ACQUISITION**
- **PROCESS CONTROL**
- **ACTIVE FILTERS**
- **TEST EQUIPMENT**
- **AUDIO**
- **WIDEBAND AMPLIFIERS**

DESCRIPTION

The OPAx365 zer∅-crossover series rail-to-rail highperformance CMOS operational amplifiers are optimized for very low voltage, single-supply applications. Rail-to-rail input/output, low-noise $(4.5nV/\sqrt{Hz})$ and high-speed operations (50MHz Gain Bandwidth) make them ideal for driving sampling analog-to-digital converters (ADCs). Applications incude audio, signal conditioning, and sensor amplification. The OPA365 family of op amps are well-suited for cell phone power amplifier control loops.

Special features include excellent common-mode rejection ratio (CMRR), no input stage crossover distortion, high input impedance and rail-to-rail input and output swing. The input common-mode range includes both the negative and positive supplies. The output voltage swing is within 10mV of the rails.

The OPA365 (single version) is available in the micro-SIZE SOT23-5 and SO-8 packages. The OPA2365 (dual version) is offered in the microSIZE DFN-8 (3mm x 3mm) and SO-8 packages. All versions are specified for operation from −40°C to +125°C. Single and dual versions have identical specifications for maximum design flexibility.

(1) Available Q3, 2006.

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ABSOLUTE MAXIMUM RATINGS(1)

- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5V beyond the supply rails should be current limited to 10mA or less.
- (3) Short-circuit to ground, one amplifier per package.

ORDERING INFORMATION(1)

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI web site at www.ti.com.

(2) Available Q3, 2006.

PIN CONFIGURATIONS

ELECTRICAL CHARACTERISTICS: **V_S = +2.2V** to +5.5V

Boldface limits apply over the specified temperature range, **TA = −40**°**C to +125**°**C.**

At T_A = +25°C, R_L = 10kΩ connected to V_S/2, V_{CM} = V_S/2, and V_{OUT} = V_S/2, unless otherwise noted.

TYPICAL CHARACTERISTICS

At $T_A = +25^{\circ}C$, $V_S = +5V$, and $C_L = 0pF$, unless otherwise noted.

OFFSET VOLTAGE DRIFT PRODUCTION DISTRIBUTION

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TYPICAL CHARACTERISTICS (continued)

At $T_A = +25$ °C, $V_S = +5V$, and $C_L = 0$ pF, unless otherwise noted.

Frequency (Hz)

TYPICAL CHARACTERISTICS (continued)

At T_A = +25°C, V_S = +5V, and C_L = 0pF, unless otherwise noted.

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APPLICATIONS INFORMATION

OPERATING CHARACTERISTICS

The OPA365 amplifier parameters are fully specified from +2.2V to +5.5V. Many of the specifications apply from −40°C to +125°C. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the Typical Characteristics.

GENERAL LAYOUT GUIDELINES

The OPA365 is a wideband amplifier. To realize the full operational performance of the device, good high-frequency printed circuit board (PCB) layout practices are required. Low-loss, 0.1µF bypass capacitors must be connected between each supply pin and ground as close to the device as possible. The bypass capacitor traces should be designed for minimum inductance.

BASIC AMPLIFIER CONFIGURATIONS

As with other single-supply op amps, the OPA365 may be operated with either a single supply or dual supplies. A typical dual-supply connection is shown in Figure 1, which is accompanied by a single-supply connection. The OPA365 is configured as a basic inverting amplifier with a gain of -10V/V. The dual-supply connection has an output voltage centered on zero, while the single− supply connection has an output centered on the common-mode voltage V_{CM} . For the circuit shown, this voltage is 1.5V, but may be any value within the commonmode input voltage range. The OPA365 V_{CM} range extends 100mV beyond the power-supply rails.

Figure 1. Basic Circuit Connections

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Figure 2 shows a single-supply, electret microphone application where V_{CM} is provided by a resistive divider. The divider also provides the bias voltage for the electret element.

INPUT AND ESD PROTECTION

The OPA365 incorporates internal electrostatic discharge (ESD) protection circuits on all pins. In the case of input and output pins, this protection primarily consists of current steering diodes connected between the input and power-supply pins. These ESD protection diodes also provide in-circuit, input overdrive protection, provided that the current is limited to 10mA as stated in the Absolute Maximum Ratings. Figure 3 shows how a series input resistor may be added to the driven input to limit the input current. The added resistor contributes thermal noise at the amplifier input and its value should be kept to the minimum in noise-sensitive applications.

RAIL−TO−RAIL INPUT

The OPA365 product family features true rail-to-rail input operation, with supply voltages as low as $\pm 1.1V$ (2.2V). A unique zer∅-crossover input topology eliminates the input offset transition region typical of many rail-to-rail, complementary stage operational amplifiers. This topology also allows the OPA365 to provide superior common−mode performance over the entire input range, which extends 100mV beyond both power-supply rails; see Figure 4. When driving ADCs, the highly linear VCM range of the OPA365 assures that the op amp/ADC system linearity performance is not compromised.

Figure 2. Microphone Preamplifier

Figure 3. Input Current Protection

Figure 4. OPA365 has Linear Offset Over the Entire Common-Mode Range

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A simplified schematic illustrating the rail-to-rail input circuitry is shown in Figure 5.

CAPACITIVE LOADS

The OPA365 may be used in applications where driving a capacitive load is required. As with all op amps, there may be specific instances where the OPA365 can become unstable, leading to oscillation. The particular op amp circuit configuration, layout, gain and output loading are some of the factors to consider when establishing whether an amplifier will be stable in operation. An op amp in the unity-gain (+1V/V) buffer configuration and driving a capacitive load exhibits a greater tendency to be unstable than an amplifier operated at a higher noise gain. The capacitive load, in conjunction with the op amp output resistance, creates a pole within the feedback loop that degrades the phase margin. The degradation of the phase margin increases as the capacitive loading increases.

When operating in the unity-gain configuration, the OPA365 remains stable with a pure capacitive load up to approximately 1nF. The equivalent series resistance (ESR) of some very large capacitors $(C_1 > 1\mu F)$ is sufficient to alter the phase characteristics in the feedback loop such that the amplifier remains stable. Increasing the amplifier closed-loop gain allows the amplifier to drive increasingly larger capacitance. This increased capability is evident when observing the overshoot response of the amplifier at higher voltage gains. See the typical characteristic graph, Small-Signal Overshoot vs. Capacitive Load.

One technique for increasing the capacitive load drive capability of the amplifier operating in unity gain is to insert a small resistor, typically 10 Ω to 20 Ω , in series with the output; see Figure 6. This resistor significantly reduces the overshoot and ringing associated with large capacitive loads. A possible problem with this technique is that a voltage divider is created with the added series resistor and any resistor connected in parallel with the capacitive load. The voltage divider introduces a gain error at the output that reduces the output swing. The error contributed by the voltage divider may be insignificant. For instance, with a load resistance, $R_1 = 10k\Omega$, and $R_S = 20\Omega$, the gain error is only about 0.2%. However, when R_L is decreased to 600 $Ω$, which the OPA365 is able to drive, the error increases to 7.5%.

Figure 5. Simplified Schematic

Figure 6. Improving Capacitive Load Drive

ACHIEVING AN OUTPUT LEVEL OF ZERO VOLTS (0V)

Certain single-supply applications require the op amp output to swing from 0V to a positive full-scale voltage and have high accuracy. An example is an op amp employed to drive a single-supply ADC having an input range from 0V to +5V. Rail-to-rail output amplifiers with very light output loading may achieve an output level within millivolts of 0V (or $+V_S$ at the high end), but not 0V. Furthermore, the deviation from 0V only becomes greater as the load current required increases. This increased deviation is a result of limitations of the CMOS output stage.

When a pull-down resistor is connected from the amplifier output to a negative voltage source, the OPA365 can achieve an output level of 0V, and even a few millivolts below 0V. Below this limit, nonlinearity and limiting conditions become evident. Figure 7 illustrates a circuit using this technique.

A pull-down current of approximately 500µA is required when OPA365 is connected as a unity-gain buffer. A practical termination voltage (V_{NEG}) is −5V, but other convenient negative voltages also may be used. The pull-down resistor R_1 is calculated from $R_L = [(V_O - V_{NEG})/(500\mu A)]$. Using a minimum output voltage (V_O) of 0V, R_L = [0V–(-5V)]/(500μA)] = 10kΩ. Keep in mind that lower termination voltages result in smaller pull-down resistors that load the output during positive output voltage excursions.

Note that this technique does not work with all op amps and should only be applied to op amps such as the OPA365 that have been specifically designed to operate in this manner. Also, operating the OPA365 output at 0V changes the output stage operating conditions, resulting in somewhat lower open-loop gain and bandwidth. Keep these precautions in mind when driving a capacitive load because these conditions can affect circuit transient response and stability.

ACTIVE FILTERING

The OPA365 is well-suited for active filter applications requiring a wide bandwidth, fast slew rate, low-noise, single-supply operational amplifier. Figure 8 shows a 500kHz, 2nd-order, low-pass filter utilizing the multiple− feedback (MFB) topology. The components have been selected to provide a maximally-flat Butterworth response. Beyond the cutoff frequency, roll-off is −40dB/dec. The Butterworth response is ideal for applications requiring predictable gain characteristics such as the anti-aliasing filter used ahead of an ADC.

Figure 7. Swing-to-Ground

Figure 8. Second-Order Butterworth 500kHz Low-Pass Filter

One point to observe when considering the MFB filter is that the output is inverted, relative to the input. If this inversion is not required, or not desired, a noninverting output can be achieved through one of these options: 1) adding an inverting amplifier; 2) adding an additional 2nd-order MFB stage; or 3) using a noninverting filter topology such as the Sallen-Key (shown in Figure 9).

MFB and Sallen-Key, low-pass and high-pass filter synthesis is quickly accomplished using TI's FilterPro program. This software is available as a free download at www.ti.com.

DRIVING AN ANALOG-TO-DIGITAL CONVERTER

Very wide common-mode input range, rail-to-rail input and output voltage capability and high speed make the

OPA365 an ideal driver for modern ADCs. Also, because it is free of the input offset transition characteristics inherent to some rail-to-rail CMOS op amps, the OPA365 provides low THD and excellent linearity throughout the input voltage swing range.

Figure 10 shows the OPA365 driving an ADS8326, 16-bit, 500kSPS converter. The amplifier is connected as a unity-gain, noninverting buffer and has an output swing to 0V, making it directly compatible with the ADC minus full-scale input level. The 0V level is achieved by powering the OPA365 V– pin with a small negative voltage established by the diode forward voltage drop. A small, signal-switching diode or Schottky diode provides a suitable negative supply voltage of −0.3 to −0.7V. The supply rail-to-rail is equal to V+, plus the small negative voltage.

Figure 9. Configured as a 3-Pole, 20kHz, Sallen-Key Filter

Figure 10. Driving the ADS8326

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One method for driving an ADC that negates the need for an output swing down to 0V uses a slightly compressed ADC full-scale input range (FSR). For example, the 16-bit ADS8361 (shown in Figure 11) has a maximum FSR of 0V to 5V, when powered by a +5V supply and V_{RFF} of 2.5V. The idea is to match the ADC input range with the op amp full linear output swing range; for example, an output range of +0.1 to +4.9V. The reference output from the ADS8361 ADC is divided down from 2.5V to 2.4V using a resistive divider. The ADC FSR then becomes $4.8V_{\text{PP}}$ centered on a common-mode voltage of +2.5V. Current from the ADS8361 reference pin is limited to about ±10µA. Here, 5µA was used to bias the divider. The resistors must be precise

to maintain the ADC gain accuracy. An additional benefit of this method is the elimination of the negative supply voltage; it requires no additional power-supply current.

An RC network, consisting of R_1 and C_1 , is included between the op amp and the ADS8361. It not only provides a high-frequency filter function, but more importantly serves as a charge reservoir used for charging the converter internal hold capacitance. This capability assures that the op amp output linearity is maintained as the ADC input characteristics change throughout the conversion cycle. Depending on the particular application and ADC, some optimization of the R_1 and C_1 values may be required for best transient performance.

Figure 11. Driving the ADS8361

Figure 12 illustrates the OPA2365 dual op amp providing signal conditioning within an ADS1258 bridge sensor circuit. It follows the ADS1258 16:1 multiplexer and is connected as a differential in/differential out amplifier. The voltage gain for this stage is approximately 10V/V. Driving the ADS1258 internal ADC in differential mode, rather than in a single-ended, exploits the full linearity performance capability of the converter. For best common-mode rejection the two R_2 resistors should be closely matched.

Note that in Figure 12, the amplifiers, bridges, ADS1258 and internal reference are powered by the same single +5V supply. This ratiometric connection helps cancel excitation voltage drift effects and noise.

For best performance, the +5V supply should be as free as possible of noise and transients.

When the ADS1258 data rate is set to maximum and the chop feature enabled, this circuit yields 12 bits of noise-free resolution with a 50mV full-scale input.

The chop feature is used to reduce the ADS1258 offset and offset drift to very low levels. A 2.2nF capacitor is required across the ADC inputs to bypass the sampling currents. The 47 Ω resistors provide isolation for the OPA2365 outputs from the relatively large, 2.2nF capacitive load. For more information regarding the ADS1258, see the product data sheet available for down load at www.ti.com.

Figure 12. Conditioning Input Signals to the ADS1258 on a Single-Supply

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PACKAGING INFORMATION

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ACTIVE: Product device recommended for new designs.

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NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

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(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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PLASTIC SMALL-OUTLINE PACKAGE

NOTES: А. All linear dimensions are in millimeters.

This drawing is subject to change without notice. **B.**

Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side. $\mathbb{C}.$

D. Falls within JEDEC MO-178 Variation AA.

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