**EVALUATION KIT**

# **MAXM**

# **Dual-Output Step-Down DC-DC Converter for PDA/Palmtop Computers AVAILABLE**

## **General Description**

The MAX1775 dual, step-down DC-DC converter generates both the main (+3.3V at over 2A) and core (+1.8V at up to 1.5A) supplies for a complete power solution for PDAs, subnotebooks, and other hand-held devices. The main output is adjustable from +1.25V to +5.5V. The core output is adjustable from 1V to 5V. Both switching converters operate at up to 1.25MHz for small external components and use synchronous rectifiers to achieve efficiencies up to 95%. Operation with up to 100% duty cycle provides the lowest possible dropout voltage to extend useful battery life.

The MAX1775 accepts inputs from +2.7V up to +28V, allowing use with many popular battery configurations as well as AC-DC wall adapters. Digital soft-start reduces battery current surges at power-up. Both the main and core converters have separate shutdown inputs. The MAX1775 comes in a small 16-pin QSOP package.

The MAX1775 evaluation kit is available to help reduce design time.

### **\_Applications**

Hand-Held Computers PDAs Internet Access Tablets POS Terminals Subnotebooks



## **MAXIM**

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**Up to 92% Efficiency** ♦ **100% (max) Duty Cycle** ♦ **Up to 1.25MHz Switching Frequency**

♦ **Dual, High-Efficiency, Synchronous Rectified**

**Adjustable from +1.25V to +5.5V**

- ♦ **Input Voltage Range from +2.7V to +28V**
- ♦ **170**μ**A Quiescent Current**
- ♦ **5**μ**A Shutdown Current**

**Step-Down Converter**

**Internal Switches Up to 1.5A Load Current**

**Over 2A Load Current Up to 95% Efficiency**

**Adjustable from 1V to 5V**

♦ **Main Power**

♦ **Core Power**

- ♦ **Digital Soft-Start**
- ♦ **Independent Shutdown Inputs**

## **Ordering Information**



# **Typical Operating Circuit**



**MAX1775 SZZIXVW** 

**Features**

**For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.**

# **MAX1775 MAX1775**

## **ABSOLUTE MAXIMUM RATINGS**



Continuous Power Dissipation



Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## **ELECTRICAL CHARACTERISTICS**

(VIN = +12V, VMAIN = VINC = VCS- = VCS+ = +3.3V, VCORE = +1.8V, Circuit of Figure 4, **TA = 0°C to +85°C,** unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .)



# **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{IN} = +12V, V_{MAIN} = V_{INC} = V_{CS} = V_{CS} + 43.3V, V_{CORE} = +1.8V,$  Circuit of Figure 4,  $T_A = 0^\circ \text{C}$  to  $+85^\circ \text{C}$ , unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .)



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# **ELECTRICAL CHARACTERISTICS (continued)**

(VIN = +12V, VMAIN = VINC = VCS- = VCS+ = +3.3V, VCORE = +1.8V, Circuit of Figure 4, **TA -40°C to +85°C,** unless otherwise noted.) (Note 2)



## **ELECTRICAL CHARACTERISTICS (continued)**

 $(V_{IN} = +12V$ ,  $V_{MAIN} = V_{INC} = V_{CS} = V_{CS} + 43.3V$ ,  $V_{CORE} = +1.8V$ , Circuit of Figure 4, **T<sub>A</sub> -40°C to +85°C,** unless otherwise noted.) (Note 2)



**Note 1:** This parameter is guaranteed based on the LXC P-channel current limit and the LXC N-channel valley current. **Note 2:** Specifications to -40°C are guaranteed by design and not production tested.



# **Typical Operating Characteristics**

(Circuit of Figure 1,  $V_{\text{MAIN}} = +3.3V$ ,  $V_{\text{CORE}} = +1.8V$ ,  $T_A = +25^{\circ}\text{C}$ , unless otherwise noted.)

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# **Typical Operating Characteristics (continued)**

(Circuit of Figure 1,  $V_{\text{MAIN}} = +3.3V$ ,  $V_{\text{CORE}} = +1.8V$ ,  $T_A = +25^{\circ}\text{C}$ , unless otherwise noted.)



**MAIN SWITCHING WAVEFORMS, HEAVY LOAD (1A)**

1μs/div

MAX1775 toc06

LX 5V/div

 $\overline{0}$ 500mA 1000mA

ILM 500mA/div

V<sub>MAIN</sub><br>(AC-COUPLED) 20mV/div



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 $\boldsymbol{0}$ 12V **MAIN LINE-TRANSIENT RESPONSE (5V TO 12V)** MAX1775 toc09 100μs/div VIN V<sub>MAIN</sub> 50mV/div 5V

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## **Typical Operating Characteristics (continued)**

(Circuit of Figure 1,  $V_{\text{MAIN}} = +3.3V$ ,  $V_{\text{CORE}} = +1.8V$ ,  $T_A = +25^{\circ}$ C, unless otherwise noted.)









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# **Pin Description**



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Figure 1. Typical Application Circuit (Low Input Voltage)

## **Detailed Description**

The MAX1775 dual step-down DC-DC converter is designed to power PDA, palmtop, and subnotebook computers. Normally, these devices need two separate power supplies—one for the processor and another higher voltage supply for the peripheral circuitry. The MAX1775 provides an adjustable +1.25V to +5.5V main output designed to power the peripheral circuitry of PDAs and similar devices. The main output delivers over 2A output current. The lower voltage core converter has an adjustable  $+1.0V$  to  $+5.0V$  output, providing up to 1.5A output current. Both regulators utilize a proprietary regulation scheme, allowing PWM operation at medium to heavy loads, and automatically switch to pulse skipping at light loads for improved efficiency. Figure 1 is the typical application circuit.

#### **Operating Modes for the Step-Down Converters**

When delivering low output currents, the MAX1775 operates in discontinuous conduction mode. Current through the inductor starts at zero, rises above the minimum current limit, then ramps down to zero during each cycle (see Typical Operating Characteristics). The switch waveform may exhibit ringing, which occurs at the resonant frequency of the inductor and stray capacitance, due to the residual energy trapped in the core when the rectifier MOSFET turns off. This does not degrade the circuit performance.

When delivering medium-to-high output currents, the MAX1775 operates in PWM continuous-conduction mode. In this mode, current always flows through the inductor and never ramps to zero. The control circuit adjusts the switch duty cycle to maintain regulation without exceeding the peak switching current set by the current-sense resistor.

#### **100% Duty Cycle and Dropout**

The MAX1775 operates with a duty cycle up to 100%. This feature extends the input voltage range by turning the MOSFET on continuously when the supply voltage approaches the output voltage. This services the load when conventional switching regulators with less than 100% duty cycle would fail. Dropout voltage is defined as the difference between the input and output voltages when the input is low enough for the output to drop out of regulation. Dropout depends on the MOS-FET drain-to-source on-resistance, current-sense resistor, and inductor series resistance, and is proportional to the load current:

> Dropout voltage = IOUT ✕ [RDS(ON) + RSENSE + RINDUCTOR]





Figure 2. Simplified Control System Block Diagram

#### **Regulation Control Scheme**

The MAX1775 has a unique operating scheme that allows PWM operation at medium and high current, with automatic switching to pulse-skipping mode at lower currents to improve light-load efficiency. Figure 2 shows a simplified block diagram.

Under medium- and heavy-load operation, the inductor current is continuous and the part operates in PWM mode. In this mode, the switching frequency is set by either the minimum on-time or the minimum off-time, depending on the duty cycle. The duty cycle is approximately the output voltage divided by the input voltage. If the duty cycle is less than 50%, the minimum on-time controls the frequency; and the frequency is approximately  $f \approx 2.5$ MHz  $\times$  D, where D is the duty cycle. If the duty cycle is greater than 50%, the minimum off-time sets the frequency; and the frequency is approximately  $f \approx 2.5$ MHz  $\times$  (1 - D).

In both cases, the voltage is regulated by the error comparator. For low duty cycles (<50%), the P-channel MOSFET turns on for the minimum on-time, causing fixed-on-time operation. During the P-channel MOSFET on-time, the output voltage rises. Once the P-channel MOSFET turns off, the voltage drops to the regulation threshold, at which time another cycle is initiated. For high duty cycles (>50%), the P-channel MOSFET remains off for the minimum off-time, causing fixed offtime operation. In this case, the P-channel MOSFET remains on until the output voltage rises to the regulation threshold. Then the P-channel MOSFET turns off for the minimum off-time, initiating another cycle.

By switching between fixed on-time and fixed off-time operation, the MAX1775 can operate at high input-output ratios, yet still operate up to 100% duty cycle for low dropout. Note that when operating in fixed on-time, the minimum output voltage is regulated; but in fixed off-time operation, the maximum output voltage is regulated. Thus, as the input voltage drops below approximately twice the output voltage, a decrease in line regulation can be expected. The drop in voltage is approximately  $V_{DROP} \approx V_{RIPPLE}$ . At light output loads, the inductor current is discontinuous, causing the MAX1775 to operate at lower frequencies, reducing the MOSFET gate drive and switching losses. In discontinuous mode, under most circumstances, the on-time will be a fixed minimum of 400ns.

The MAX1775 features four separate current-limit threshold detectors and a watchdog timer for each of its step-down converters. In addition to the more common peak current detector and zero crossing detector, each converter also provides a valley current detector (IVALLEY) and a minimum current detector (IMIN). IVALLEY is used to force the inductor current to drop to a lower level after hitting peak current before allowing the Pchannel MOSFET to turn on. This is a safeguard against inductor current significantly overshooting above the peak current when the inductor discharges too slowly when VOUT/L is small. IMIN is useful in ensuring that a minimum current is built up in the inductor before turning off the P-channel MOSFET. This helps the inductor to charge the output near dropout when dI/dt is small (because ( $V_{IN}$  -  $V_{OUT}$ ) / L is small) to avoid multiple **MAX1775**



Figure 3. Simplified Block Diagram

pulses and low efficiency. This feature, however, is disabled during dropout and light-load conditions where the inductor current may take too long to reach the IMIN value. A watchdog timer overrides IMIN after the Pchannel MOSFET has been on for longer than about 10µs.

#### **Main Step-Down Converter**

The main step-down converter features adjustable +1.25V to +5.5V output, delivering over 2A from a +2.7V to +28V input (see Setting the Output Voltages). The use of external MOSFETs and a current-sense resistor maximizes design flexibility. The MAX1775 offers a synchronous rectifier MOSFET driver that improves efficiency by eliminating losses through a diode. The two MOSFET drive outputs, PDRV and NDRV, control these external MOSFETs. The output swing of these outputs is limited to reduce power con-

sumption by limiting the amount of injected gate charge (see Internal Linear Regulators). The main current limit is sensed through a small sense resistor at the converter output (see Setting the Current Limit). Driving SHDNM low puts the main converter in a low-power shutdown mode. The core regulator is still functional when the main converter is in shutdown.

#### **Core Step-Down Converter**

The core step-down converter produces a +1.0V to +5.0V output from a +2.6V to +5.5V input. The low-voltage input allows the use of internal power MOSFETs, taking advantage of their low  $R_{DS(ON)}$ , improving efficiency and reducing board space. Like the main converter, the core regulator makes use of an N-channel MOSFET synchronous rectifier, improving efficiency and eliminating the need for an external Schottky diode. Current sensing is internal to the device, eliminating the need for an external sense resistor. The maximum and minimum current limits are sensed through the P-channel MOSFET, while the valley current and zero crossing current are sensed through the N-channel MOSFET. The core output voltage is measured at FBC through a resistive voltagedivider. This divider can be adjusted to set the output voltage level (see Setting the Output Voltages). The core input can be supplied from the main regulator or an external supply that does not exceed +5.5V (see High-Voltage Configuration and Low-Voltage Configuration). The core converter can be shut down independent of the main converter by driving **SHDNC** low. If the main converter output is supplying power to the core and is shut down, SHDNM controls both outputs. Figure 3 is a simplified block diagram.

#### **Internal Linear Regulators**

There are two linear regulators internal to the MAX1775. A high-voltage linear regulator accepts inputs up to +28V, reducing it to +2.8V at CVL to provide power to the MAX1775. Once the voltage at CS- reaches +2.47V, CVL is switched to CS, allowing it to be driven from the main converter, improving efficiency. CVL supplies the internal bias to the IC and power for the NDRV gate driver.

The CVH regulator provides the low-side voltage for the main regulator's PDRV output. The voltage at CVH is regulated at 4.3V below  $V_{\text{IN}}$  to limit the voltage swing on PDRV, reducing gate charge and improving efficiency (Figure 3).

#### **Reference**

The MAX1775 has an accurate internally trimmed +1.25V reference at REF. REF can source no more than 50µA. Bypass REF to GND with a 0.22µF capacitor.



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Figure 4. High Input Voltage Cascaded Configuration

## **Design Procedure**

#### **Low-Voltage Configuration**

To improve efficiency and conserve board space, the core regulator operates from low input voltages, taking advantage of internal low-voltage, low-on-resistance MOSFETs. When the input voltage remains below 5.5V, run the core converter directly from the input by connecting INC to IN (Figure 1). This configuration takes advantage of the core's low-voltage design and improves efficiency.

#### **High-Voltage Configuration**

For input voltages greater than 5.5V, cascade the main and core converters by connecting INC to the main output voltage. In this configuration (Figure 4), the core converter is powered from the main output. Ensure that the main output can simultaneously supply its load and the core input current. In this configuration, the main output voltage must be set above the 2.6V minimum input voltage of the core converter.

#### **Setting the Output Voltages**

The main output voltage may be set from +1.25V and +5.5V with two external resistors connected as a voltage-divider to FBM (Figure 1). Resistor values can be calculated by the following equation:

R2 = R3 ✕ [(VOUTM / VFBM) - 1]

where VFBM =  $+1.25V$ . Choose R3 to be 40kΩ or less.

The core regulator output is adjustable from +1.0V to +5.0V through two external resistors connected as a voltage-divider to FBC (Figure 1). Resistor values can be calculated through the following equation:

$$
R4 = R5 \times [(VOUTC / VFBC) - 1]
$$

where V<sub>FBC</sub> = +1.0V. Choose R5 to be 30kΩ or less.

#### **Setting the Current Limit**

The main regulator current limit is set externally through a small current-sense resistor, R1 (Figure 1). The value of R1 can be calculated by the following equation:

$$
R1 = \frac{V_{CLM}}{\left(1.3 \text{ I}_{OUT}\right)}
$$

where  $VCLM = 80mV$  is the current-sense threshold, and  $I_{\text{OUT}}$  is the current delivered to the output. The core converter current limit is set internally and cannot be modified.

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Careful layout of the current-sense signal traces is imperative. Place R1 as close to the MAX1775 as possible. The two traces should have matching length and width, be as far as possible from noisy switching signals, and be close together to improve noise rejection. These traces should be used for current-sense signal routing only and should not carry any load current. Refer to the MAX1775 Evaluation Kit for layout examples.

#### **Inductor Selection**

The essential parameters for inductor selection are inductance and current rating. The MAX1775 operates with a wide range of inductance values.

Calculate the inductance value for either core or main, LMIN:

 $L_{MIN} = (V_{IN} - V_{OUT}) \times T_{ONMIN} / I_{RIPPI F}$ 

where TONMIN is typically 400ns, and IRIPPLE is the continuous conduction ripple current. In continuous conduction, IRIPPLE should be chosen to be 30% of the maximum load current. With high inductor values, the MAX1775 begins continuous-conduction operation at a lower fraction of full load (see Detailed Description).

The inductor's saturation current must be greater than the peak switching current to prevent core saturation. Saturation occurs when the inductor's magnetic flux density reaches the maximum level the core can support, and inductance starts to fall. The inductor heating current rating must be greater than the maximum load current to prevent overheating. For optimum efficiency, the inductor series resistance should be less than the current-sense resistance.

#### **Capacitor Selection**

Choose output filter capacitors to service the output ripple current with acceptable voltage ripple. ESR in the output capacitor is a major contributor to output ripple. For the main converter, low-ESR capacitors such as polymer, ceramic, or even tantalum are recommended. For the core converter, choosing a low-ESR tantalum capacitor with enough ESR to generate about 1% ripple voltage across the output is helpful in ensuring stability.

Voltage ripple is the sum of contributions from ESR and the capacitor value:

VRIPPLE ≈ VRIPPLE,ESR + VRIPPLE,C

For tantalum capacitors, the ripple is determined mostly by the ESR. Voltage ripple due to ESR is:

```
VRIPPLE,ESR ≈ RESR ✕ IRIPPLE
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For ceramic capacitors, the ripple is mostly due to the capacitance. The ripple due to the capacitance is approximately:

VRIPPLE C  $\approx$  L IRIPPLE<sup>2</sup> / 2COUTVOUT

where  $V_{\text{OUT}}$  is the average output voltage. From this equation, estimate the output capacitor values for given voltage ripple as follows:

 $C_{\text{OUT}} = 1/2 \times L \text{ IRIPPLE}^2 / (\text{VRIPPLE}, \text{COUT} \times \text{VOUT})$ 

This equation is suitable for initial capacitor selection. Final values should be set by testing a prototype or evaluation kit. When using tantalum capacitors, use good soldering practices to prevent excessive heat from damaging the devices and increasing their ESR. Also, ensure that the tantalum capacitors' surge-current ratings exceed the startup inrush and peak switching currents.

The input filter capacitor reduces peak currents drawn from the power source and reduces noise and voltage ripple at IN, caused by the circuit's switching. Use a low-ESR capacitor. Two smaller-value low-ESR capacitors can be connected in parallel if necessary. Choose input capacitors with working voltage ratings higher than the maximum input voltage. Typically 4µF of input capacitance for every 1A of load current is sufficient. More capacitance may improve battery life and noise immunity.

Place a surface-mount ceramic capacitor at IN very close to the source of the high-side P-channel MOSFET. This capacitor bypasses the MAX1775, minimizing the effects of spikes and ringing on the MAX1775's operation.

Bypass REF with 0.22µF or greater. Place this capacitor within 0.2in (5mm) of the IC, next to REF, with a direct trace to GND.

#### **MOSFET Selection**

The MAX1775 drives an external enhancement-mode P-channel MOSFET and a synchronous-rectifier Nchannel MOSFET. When selecting the MOSFETs, important parameters to consider are on-resistance (RDS(ON)), maximum drain-to-source voltage (VDS(MAX)), maximum gate-to-source voltage (VGS(MAX)), and minimum threshold voltage (VTH(MIN)).

# **Chip Information**

PROCESS: BiCMOS

## **Package Information**

For the latest package outline information and land patterns, go to **www.maxim-ic.com/packages**.



# **Revision History**



Maxim cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Maxim product. No circuit patent licenses are implied. Maxim reserves the right to change the circuitry and specifications without notice at any time.

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