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# **LMP770x Precision, CMOS Input, RRIO, Wide Supply Range Amplifiers**

**Technical** [Documents](#page-31-0)

- Unless Otherwise Noted,
- <span id="page-0-3"></span>
- µV (Maximum) applications.
- 
- 
- 
- 
- 
- 
- 
- Supply Current (LMP7701): 715 µA
- Supply Current (LMP7702): 1.5 mA
- **Supply Current (LMP7704): 2.9 mA**
- Supply Voltage Range: 2.7 V to 12 V
- Rail-to-Rail Input and Output

# <span id="page-0-2"></span>**2 Applications**

- High Impedance Sensor Interface
- Battery-Powered Instrumentation
- <span id="page-0-0"></span>**High Gain Amplifiers**
- DAC Buffer
- Instrumentation Amplifier
- **Active Filters**

# <span id="page-0-1"></span>**1 Features 3 Description**

Tools & **[Software](#page-31-0)** 

The LMP770x are single, dual, and quad low-offset  $V_s$  voltage, rail-to-rail input and output precision Typical Values at  $V_s = 5$  V amplifiers, each with a CMOS input stage and a wide Input Offset Voltage (LMP7701):  $\pm 200 - \mu V$ <br>
with a supply voltage range. The LMP770x are part of the<br>
I MPTM precision amplifier family and are ideal for  $LMP<sup>TM</sup>$  precision amplifier family and are ideal for sensor interface and other instrumentation • Input Offset Voltage (LMP7702/LMP7704): ±220- sensor interface and other instrumentation

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• Input Bias Current: ±200 fA The specified low-offset voltage of less than ±200 µV, Input Bias Current: ±200 fA<br>
along with the specified low input bias current of less<br>
than ±1 pA, make the LMP7701 ideal for precision than  $\pm$ 1 pA, make the LMP7701 ideal for precision input Voltage Noise: 9 nV/√Hz applications. The LMP770x are built using VIP50<br>CMRR: 130 dB applications. The LMP770x are built using VIP50 technology, which allows the combination of a CMOS • Open-Loop Gain: 130 dB input stage and a 12-V common-mode and supply Temperature Range: −40°C to 125°C voltage\_range. This makes the LMP770x ideal for applications where conventional CMOS parts cannot Unity-Gain Bandwidth: 2.5 MHz operate under the desired voltage conditions.



# **Device Information[\(1\)](#page-0-0)**

(1) For all available packages, see the orderable addendum at

### **Typical Application Schematic**





# **Table of Contents**



# <span id="page-1-0"></span>**4 Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

### **Changes from Revision H (March 2013) to Revision I Page**

12.5 Glossary .. [32](#page-31-5) **8 Detailed Description** .. [21](#page-20-2) **13 Mechanical, Packaging, and Orderable** 8.1 Overview ... [21](#page-20-3)

### • Added *ESD Ratings* table, *Feature Description* section, *Device Functional Modes*, *Application and Implementation* section, *Power Supply Recommendations* section, *Layout* section, *Device and Documentation Support* section, and *Mechanical, Packaging, and Orderable Information* section. .. [1](#page-0-3)

# **Changes from Revision G (March 2013) to Revision H Page** • Changed layout of National Data Sheet to TI format ... [27](#page-26-1)

**EXAS STRUMENTS** 



# <span id="page-2-0"></span>**5 Description (continued)**

The LMP770x each have a rail-to-rail input stage that significantly reduces the CMRR glitch commonly associated with rail-to-rail input amplifiers. This is achieved by trimming both sides of the complimentary input stage, thereby reducing the difference between the NMOS and PMOS offsets. The output of the LMP770x swings within 40 mV of either rail to maximize the signal dynamic range in applications requiring low supply voltage.

The LMP7701 is offered in the space-saving 5-Pin SOT-23 and 8-Pin SOIC package. The LMP7702 is offered in the 8-Pin SOIC and 8-Pin VSSOP package. The quad LMP7704 is offered in the 14-Pin SOIC and 14-Pin TSSOP package. These small packages are ideal solutions for area constrained PC boards and portable electronics.

# <span id="page-2-1"></span>**6 Pin Configuration and Functions**





**Pin Functions - LMP7701**



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### **Pin Functions - LMP7702**







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### **Pin Functions - LMP7704**



# <span id="page-4-0"></span>**7 Specifications**

### <span id="page-4-1"></span>**7.1 Absolute Maximum Ratings**

See (1)(2)



(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *[Recommended](#page-5-0) Operating [Conditions](#page-5-0)* . Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

If Military/Aerospace specified devices are required, contact the TI Sales Office/ Distributors for availability and specifications.

(3) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.

# <span id="page-4-2"></span>**7.2 ESD Ratings**



(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) Human Body Model, applicable std. MIL-STD-883, Method 3015.7. Machine Model, applicable std. JESD22-A115-A (ESD MM std. of JEDEC) Field-Induced Charge-Device Model, applicable std. JESD22-C101-C (ESD FICDM std. of JEDEC).

(3) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

# **[LMP7701](http://www.ti.com/product/lmp7701?qgpn=lmp7701), [LMP7702,](http://www.ti.com/product/lmp7702?qgpn=lmp7702) [LMP7704](http://www.ti.com/product/lmp7704?qgpn=lmp7704)**

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### <span id="page-5-0"></span>**7.3 Recommended Operating Conditions**



(1) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.

## <span id="page-5-1"></span>**7.4 Thermal Information**



(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report ([SPRA953](http://www.ti.com/lit/pdf/spra953)).

(2) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.

# <span id="page-5-2"></span>**7.5 Electrical Characteristics 3-V**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 3 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sup>+</sup>/2, and R<sub>L</sub> > 10 kΩ to V<sup>+</sup>/2.<sup>(1)</sup>



(1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J$  >  $T_A$ .

(2) Limits are 100% production tested at 25°C. Limits over the operating temperature range are specified through correlations using the Statistical Quality Control (SQC) method.

(3) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not specified on shipped production material.

- (4) This parameter is specified by design and/or characterization and is not tested in production.
- (5) Positive current corresponds to current flowing into the device.
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# **Electrical Characteristics 3-V (continued)**





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# **Electrical Characteristics 3-V (continued)**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 3 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sup>+</sup>/2, and R<sub>L</sub> > 10 kΩ to V<sup>+</sup>/2.<sup>[\(1\)](#page-7-0)</sup>



<span id="page-7-0"></span>(6) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.<br>(7) The short circuit test is a momentary test.

(8) The number specified is the slower of positive and negative slew rates.

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### <span id="page-8-0"></span>**7.6 Electrical Characteristics 5-V**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 5 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sup>+</sup>/2, and R<sub>L</sub> > 10 kΩ to V<sup>+</sup>/2.<sup>(1)</sup>



- (1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J > T_A$ .
- (2) Limits are 100% production tested at 25°C. Limits over the operating temperature range are specified through correlations using the Statistical Quality Control (SQC) method.
- (3) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not ensured on shipped production material.
- (4) This parameter is specified by design and/or characterization and is not tested in production.
- (5) Positive current corresponds to current flowing into the device.

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# **Electrical Characteristics 5-V (continued)**





(6) The maximum power dissipation is a function of T<sub>J(MAX)</sub>, θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.<br>(7) The short circuit test is a momentary test.

- (8) The number specified is the slower of positive and negative slew rates.
- 

## **Electrical Characteristics 5-V (continued)**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 5 V, V<sup>-</sup> = 0 V, V<sub>CM</sub> = V<sup>+</sup>/2, and R<sub>L</sub> > 10 kΩ to V<sup>+</sup>/2.<sup>[\(1\)](#page-10-1)</sup>



## <span id="page-10-1"></span><span id="page-10-0"></span>**7.7 Electrical Characteristics ±5-V**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 5 V, V<sup>-</sup> = -5 V, V<sub>CM</sub> = 0 V, and R<sub>L</sub> > 10 kΩ to 0 V.<sup>(1)</sup>



- (1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J > T_A$ .
- (2) Limits are 100% production tested at 25°C. Limits over the operating temperature range are specified through correlations using the Statistical Quality Control (SQC) method.
- (3) Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not ensured on shipped production material.
- (4) This parameter is specified by design and/or characterization and is not tested in production.
- (5) Positive current corresponds to current flowing into the device.

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# **Electrical Characteristics ±5-V (continued)**





(6) The maximum power dissipation is a function of T<sub>J(MAX)</sub>, θ<sub>JA</sub>. The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC Board.<br>(7) The short circuit test is a momentary test.



## **Electrical Characteristics ±5-V (continued)**

Unless otherwise specified, all limits are ensured for T<sub>A</sub> = 25°C, V<sup>+</sup> = 5 V, V<sup>-</sup> = -5 V, V<sub>CM</sub> = 0 V, and R<sub>L</sub> > 10 kΩ to 0 V.<sup>[\(1\)](#page-12-0)</sup>



<span id="page-12-0"></span>(8) The number specified is the slower of positive and negative slew rates.

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# **7.8 Typical Characteristics**

<span id="page-13-0"></span>





### **Typical Characteristics (continued)**



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# **Typical Characteristics (continued)**





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### **Typical Characteristics (continued)**



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## **Typical Characteristics (continued)**





### **Typical Characteristics (continued)**





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# **Typical Characteristics (continued)**

 $T_A = 25^{\circ}$ C, V<sub>CM</sub> = V<sub>S</sub>/2, R<sub>L</sub> > 10 kΩ (unless otherwise noted)



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# <span id="page-20-2"></span>**8 Detailed Description**

# <span id="page-20-3"></span>**8.1 Overview**

The LMP770x are single, dual, and quad low offset voltage, rail-to-rail input and output precision amplifiers each with a CMOS input stage and wide supply voltage range of 2.7V to 12V. The LMP770x have a very low input bias current of only ±200 fA at room temperature.

The wide supply voltage range of 2.7V to 12V over the extensive temperature range of −40°C to 125°C makes the LMP770x excellent choices for low voltage precision applications with extensive temperature requirements.

The LMP770x have only ±37 μV of typical input referred offset voltage and this offset is specified to be less than ±500 μV for the single and ±520 μV for the dual and quad, over temperature. This minimal offset voltage allows more accurate signal detection and amplification in precision applications.

The low input bias current of only ±200 fA along with the low input referred voltage noise of 9 nV/√Hz gives the LMP770x superiority for use in sensor applications. Lower levels of noise from the LMP770x mean of better signal fidelity and a higher signal-to-noise ratio.

Texas Instruments is heavily committed to precision amplifiers and the market segment they serve. Technical support and extensive characterization data is available for sensitive applications or applications with a constrained error budget.

The LMP7701 is offered in the space saving 5-Pin SOT-23 and 8-Pin SOIC package. The LMP7702 comes in the 8-Pin SOIC and 8-Pin VSSOP package. The LMP7704 is offered in the 14-Pin SOIC and 14-Pin TSSOP package. These small packages are ideal solutions for area constrained PC boards and portable electronics.

# <span id="page-20-0"></span>**8.2 Functional Block Diagram**



**Figure 40. Functional Block Diagram (LMP7701)**

# <span id="page-20-1"></span>**8.3 Feature Description**

### **8.3.1 Capacitive Load**

The LMP770x can each be connected as a non-inverting unity gain follower. This configuration is the most sensitive to capacitive loading.

The combination of a capacitive load placed on the output of an amplifier along with the amplifier's output impedance creates a phase lag which in turn reduces the phase margin of the amplifier. If the phase margin is significantly reduced, the response will be either underdamped or it will oscillate.

To drive heavier capacitive loads, an isolation resistor,  $R_{\text{ISO}}$ , in [Figure](#page-21-0) 41 should be used. By using this isolation resistor, the capacitive load is isolated from the amplifier's output, and hence, the pole caused by  $C_{L}$  is no longer in the feedback loop. The larger the value of  $R_{\rm ISO}$ , the more stable the output voltage will be. If values of  $R_{\rm ISO}$  are sufficiently large, the feedback loop will be stable, independent of the value of C<sub>L</sub>. However, larger values of R<sub>ISO</sub> result in reduced output swing and reduced output current drive.

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### **Feature Description (continued)**



**Figure 41. Isolating Capacitive Load**

### <span id="page-21-0"></span>**8.3.2 Input Capacitance**

CMOS input stages inherently have low input bias current and higher input referred voltage noise. The LMP770x enhance this performance by having the low input bias current of only  $\pm 200$  fA, as well as, a very low input referred voltage noise of 9 nV/√Hz. To achieve this a larger input stage has been used. This larger input stage increases the input capacitance of the LMP770x. The typical value of this input capacitance,  $C_{IN}$ , for the LMP770x is 25 pF. The input capacitance will interact with other impedances such as gain and feedback resistors, which are seen on the inputs of the amplifier, to form a pole. This pole will have little or no effect on the output of the amplifier at low frequencies and DC conditions, but will play a bigger role as the frequency increases. At higher frequencies, the presence of this pole will decrease phase margin and will also cause gain peaking. To compensate for the input capacitance, care must be taken in choosing the feedback resistors. In addition to being selective in picking values for the feedback resistor, a capacitor can be added to the feedback path to increase stability.

The DC gain of the circuit shown in [Figure](#page-21-1) 42 is simply  $-R_2/R_1$ .





<span id="page-21-1"></span>For the time being, ignore  $C_F$ . The AC gain of the circuit in [Figure](#page-21-1) 42 can be calculated as follows:

$$
\frac{V_{OUT}}{V_{IN}}(s) = \frac{-R_2/R_1}{\left[1 + \frac{s}{\left(\frac{A_0 R_1}{R_1 + R_2}\right)} + \frac{s^2}{\left(\frac{A_0}{C_{IN} R_2}\right)}\right]}
$$

<span id="page-21-2"></span>This equation is rearranged to find the location of the two poles:

$$
P_{1,2} = \frac{-1}{2C_{IN}} \left[ \frac{1}{R_1} + \frac{1}{R_2} \pm \sqrt{\left(\frac{1}{R_1} + \frac{1}{R_2}\right)^2 - \frac{4 A_0 C_{IN}}{R_2}} \right]
$$

(2)

(1)



### **Feature Description (continued)**

As shown in [Equation](#page-21-2) 2, as values of  $R_1$  and  $R_2$  are increased, the magnitude of the poles is reduced, which in turn decreases the bandwidth of the amplifier. Whenever possible, it is best to choose smaller feedback resistors. [Figure](#page-22-0) 43 shows the effect of the feedback resistor on the bandwidth of the LMP770x.



**Figure 43. Closed-Loop Gain vs Frequency**

<span id="page-22-0"></span>[Equation](#page-21-2) 2 has two poles. In most cases, it is the presence of pairs of poles that causes gain peaking. To eliminate this effect, the poles should be placed in Butterworth position, because poles in Butterworth position do not cause gain peaking. To achieve a Butterworth pair, the quantity under the square root in [Equation](#page-21-2) 2 should be set to equal −1. Using this fact and the relation between R<sub>1</sub> and R<sub>2</sub>, R<sub>2</sub> = −A<sub>V</sub> R<sub>1</sub>, the optimum value for R<sub>1</sub> can be found. This is shown in [Equation](#page-22-1) 3. If R<sub>1</sub> is chosen to be larger than this optimum value, gain peaking will occur.

$$
R_1<\frac{\left(1-A_V\right)^2}{2A_0A_VC_{IN}}
$$

(3)

<span id="page-22-1"></span>In [Figure](#page-21-1) 42,  $C_F$  is added to compensate for input capacitance and to increase stability. Additionally,  $C_F$  reduces or eliminates the gain peaking that can be caused by having a larger feedback resistor. [Figure](#page-22-2) 44 shows how  $C_F$ reduces gain peaking.



<span id="page-22-2"></span>**Figure 44. Closed-Loop Gain vs Frequency With Compensation**



### **Feature Description (continued)**

### **8.3.3 Diodes Between the Inputs**

<span id="page-23-0"></span>The LMP770x have a set of anti-parallel diodes between the input pins, as shown in [Figure](#page-23-0) 45. These diodes are present to protect the input stage of the amplifier. At the same time, they limit the amount of differential input voltage that is allowed on the input pins. A differential signal larger than one diode voltage drop might damage the diodes. The differential signal between the inputs needs to be limited to ±300 mV or the input current needs to be limited to ±10 mA.



**Figure 45. Input of LMP7701**



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### <span id="page-24-0"></span>**8.4 Device Functional Modes**

### **8.4.1 Precision Current Source**

The LMP770x can each be used as a precision current source in many different applications. [Figure](#page-24-3) 46 shows a typical precision current source. This circuit implements a precision voltage controlled current source. Amplifier A1 is a differential amplifier that uses the voltage drop across  $R_s$  as the feedback signal. Amplifier A2 is a buffer that eliminates the error current from the load side of the  $R<sub>S</sub>$  resistor that would flow in the feedback resistor if it were connected to the load side of the  $R<sub>S</sub>$  resistor. In general, the circuit is stable as long as the closed loop bandwidth of amplifier A2 is greater then the closed loop bandwidth of amplifier A1. If A1 and A2 are the same type of amplifiers, then the feedback around A1 will reduce its bandwidth compared to A2.



**Figure 46. Precision Current Source**

<span id="page-24-4"></span><span id="page-24-3"></span>The equation for output current can be derived as shown in [Equation](#page-24-4) 4.

$$
\frac{V_2R}{R+R} + \frac{(V_0 - IR_3)R}{R+R} = \frac{V_1R}{R+R} + \frac{V_0R}{R+R}
$$

<span id="page-24-5"></span>Solving for the current I results in the [Equation](#page-24-5) 5.

$$
I = \frac{V_2 - V_1}{R_S}
$$

(4)

(5)

### <span id="page-24-1"></span>**9 Application and Implementation**

### **NOTE**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### <span id="page-24-2"></span>**9.1 Application Information**

### **9.1.1 Low Input Voltage Noise**

The LMP770x have the very low input voltage noise of 9 nV/√Hz. This input voltage noise can be further reduced by placing N amplifiers in parallel as shown in [Figure](#page-25-0) 47. The total voltage noise on the output of this circuit is divided by the square root of the number of amplifiers used in this parallel combination. This is because each individual amplifier acts as an independent noise source, and the average noise of independent sources is the quadrature sum of the independent sources divided by the number of sources. For N identical amplifiers, this means:



(6)

### **Application Information (continued)**

REDUCED INPUT VOLTAGE NOISE =  $\frac{1}{N} \sqrt{\frac{e_{n1}^2 + e_{n2}^2 + \cdots + e_{nN}^2}{2}}$  $=\frac{1}{11}$ N  $\frac{1}{N}\sqrt{Ne_n^2} = \frac{\sqrt{N}}{N}$  $\frac{1}{N}$  e<sub>n</sub>  $=\frac{1}{\sqrt{\mathsf{N}}}\,$  e<sub>n</sub>

[Figure](#page-25-0) 47 shows a schematic of this input voltage noise reduction circuit. Typical resistor values are:  $R_G$  = 10Ω,  $R_F$  = 1 kΩ, and  $R_O$  = 1 kΩ.



**Figure 47. Noise Reduction Circuit**

### <span id="page-25-0"></span>**9.1.2 Total Noise Contribution**

The LMP770x have very low input bias current, very low input current noise, and very low input voltage noise. As a result, these amplifiers are ideal choices for circuits with high impedance sensor applications.

[Figure](#page-26-2) 48 shows the typical input noise of the LMP770x as a function of source resistance where:

 $e_n$  denotes the input referred voltage noise

 ${\sf e}_{\sf i}$  is the voltage drop across source resistance due to input referred current noise or  ${\sf e}_{\sf i}$  =  ${\sf R}_{\sf S}$  \* i<sub>n</sub>

 $e<sub>t</sub>$  shows the thermal noise of the source resistance

 $e_{ni}$  shows the total noise on the input.

Where:

$$
e_{ni} = \sqrt{e_n^2 + e_i^2 + e_t^2}
$$



### **Application Information (continued)**

The input current noise of the LMP770x is so low that it will not become the dominant factor in the total noise unless source resistance exceeds 300 MΩ, which is an unrealistically high value.

As is evident in [Figure](#page-26-2) 48, at lower  $R_S$  values, total noise is dominated by the amplifier's input voltage noise. Once  $R_S$  is larger than a few kilo-Ohms, then the dominant noise factor becomes the thermal noise of  $R_S$ . As mentioned before, the current noise will not be the dominant noise factor for any practical application.



**Figure 48. Total Input Noise**

# <span id="page-26-2"></span><span id="page-26-1"></span><span id="page-26-0"></span>**9.2 Typical Application**



<span id="page-26-3"></span>

**STRUMENTS** 

### **Typical Application (continued)**

### **9.2.1 Design Requirements**

pH electrodes are very high impedance sensors. As their name indicates, they are used to measure the pH of a solution. They usually do this by generating an output voltage which is proportional to the pH of the solution. pH electrodes are calibrated so that they have zero output for a neutral solution,  $pH = 7$ , and positive and negative voltages for acidic or alkaline solutions. This means that the output of a pH electrode is bipolar and must be level shifted to be used in a single supply system. The rate of change of this voltage is usually shown in mV/pH and is different for different pH sensors. Temperature is also an important factor in a pH electrode reading. The output voltage of the senor will change with temperature.

### **9.2.2 Detailed Design Procedure**

Many sensors have high source impedances that may range up to 10 MΩ. The output signal of sensors often needs to be amplified or otherwise conditioned by means of an amplifier. The input bias current of this amplifier can load the sensor's output and cause a voltage drop across the source resistance as shown in [Figure](#page-27-0) 50, where  $V_{IN}^+ = V_S - I_{BIAS}^*R_S$ 

The last term,  $I_{BIAS}R_S$ , shows the voltage drop across  $R_S$ . To prevent errors introduced to the system due to this voltage, an op amp with very low input bias current must be used with high impedance sensors. This is to keep the error contribution by  $I_{BIAS}$ <sup>\*</sup>R<sub>S</sub> less than the input voltage noise of the amplifier, so that it will not become the dominant noise factor.



**Figure 50. Noise Due to IBIAS** 

<span id="page-27-0"></span>[Figure](#page-27-1) 51 shows a typical output voltage spectrum of a pH electrode. The exact values of output voltage will be different for different sensors. In this example, the pH electrode has an output voltage of 59.15 mV/pH at 25°C.



**Figure 51. Output Voltage of a pH Electrode**

<span id="page-27-1"></span>The temperature dependence of a typical pH electrode is shown in [Figure](#page-28-0) 52. As is evident, the output voltage changes with changes in temperature.

The schematic shown in [Figure](#page-26-3) 49 is a typical circuit which can be used for pH measurement. The LM35 is a precision integrated circuit temperature sensor. This sensor is differentiated from similar products because it has an output voltage linearly proportional to Celcius measurement, without converting the temperature to Kelvin. The LM35 is used to measure the temperature of the solution and feeds this reading to the Analog to Digital Converter, ADC. This information is used by the ADC to calculate the temperature effects on the pH readings. The LM35 needs to have a resistor, R<sub>T</sub> in [Figure](#page-26-3) 49, to  $-V^*$  to be able to read temperatures less than 0°C. R<sub>T</sub> is not needed if temperatures are not expected to be less than zero.



### **Typical Application (continued)**

The output of pH electrodes is usually large enough that it does not require much amplification; however, due to the very high impedance, the output of a pH electrode needs to be buffered before it can go to an ADC. Because most ADCs are operated on single supply, the output of the pH electrode also needs to be level shifted. Amplifier A1 buffers the output of the pH electrode with a moderate gain of  $+2$ , while A2 provides the level shifting. V<sub>OUT</sub> at the output of A2 is given by:  $V_{\text{OUT}} = -2V_{\text{DH}} + 1.024V$ .

The LM4140A is a precision, low noise, voltage reference used to provide the level shift needed. The ADC used in this application is the ADC12032 which is a 12-bit, 2 channel converter with multiplexers on the inputs and a serial output. The 12-bit ADC enables users to measure pH with an accuracy of 0.003 of a pH unit. Adequate power supply bypassing and grounding is extremely important for ADCs. Recommended bypass capacitors are shown in [Figure](#page-26-3) 49. It is common to share power supplies between different components in a circuit. To minimize the effects of power supply ripples caused by other components, the op amps must have bypass capacitors on the supply pins. Using the same value capacitors as those used with the ADC are ideal. The combination of these three values of capacitors ensures that AC noise present on the power supply line is grounded and does not interfere with the amplifiers' signal.

### **9.2.3 Application Curves**



<span id="page-28-0"></span>**Figure 52. Temperature Dependence of a pH Electrode**



# <span id="page-29-0"></span>**10 Power Supply Recommendations**

For proper operation, the power supplies must be decoupled. For supply decoupling, TI recommends placing 10-nF to 1-µF capacitors as close as possible to the operational-amplifier power supply pins. For single supply configurations, place a capacitor between the V<sup>+</sup> and V<sup>-</sup> supply pins. For dual supply configurations, place one capacitor between V<sup>+</sup> and ground, and place a second capacitor between V<sup>-</sup> and ground. Bypass capacitors must have a low ESR of less than 0.1 Ω.



# <span id="page-30-0"></span>**11 Layout**

### <span id="page-30-1"></span>**11.1 Layout Guidelines**

Take care to minimize the loop area formed by the bypass capacitor connection between supply pins and ground. A ground plane underneath the device is recommended; any bypass components to ground should have a nearby via to the ground plane. The optimum bypass capacitor placement is closest to the corresponding supply pin. Use of thicker traces from the bypass capacitors to the corresponding supply pins will lower the power supply inductance and provide a more stable power supply.

The feedback components should be placed as close to the device as possible to minimize stray parasitics.

### **11.2 Layout Example**

<span id="page-30-2"></span>

**Figure 53. LMP7701 Example Layout**

# <span id="page-31-1"></span>**12 Device and Documentation Support**

## <span id="page-31-0"></span>**12.1 Related Links**

**[LMP7701](http://www.ti.com/product/lmp7701?qgpn=lmp7701), [LMP7702,](http://www.ti.com/product/lmp7702?qgpn=lmp7702) [LMP7704](http://www.ti.com/product/lmp7704?qgpn=lmp7704)**

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.



### **Table 1. Related Links**

### <span id="page-31-2"></span>**12.2 Community Resources**

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms](http://www.ti.com/corp/docs/legal/termsofuse.shtml) of [Use.](http://www.ti.com/corp/docs/legal/termsofuse.shtml)

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**Design [Support](http://support.ti.com/)** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### <span id="page-31-3"></span>**12.3 Trademarks**

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# <span id="page-31-4"></span>**12.4 Electrostatic Discharge Caution**



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

# <span id="page-31-5"></span>**12.5 Glossary**

[SLYZ022](http://www.ti.com/lit/pdf/SLYZ022) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

# <span id="page-31-6"></span>**13 Mechanical, Packaging, and Orderable Information**

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.





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# **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.



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**OBSOLETE:** TI has discontinued the production of the device.

**(2)** Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent>for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures. TI Pb-Free products are suitable for use in specified lead-free processes. Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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# **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**





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DBV (R-PDSO-G5)

PLASTIC SMALL-OUTLINE PACKAGE



- A. All linear dimensions are in millimeters.
	- This drawing is subject to change without notice. **B.**
	- Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side. C.
	- D. Falls within JEDEC MO-178 Variation AA.





NOTES:

- A. All linear dimensions are in millimeters. B. This drawing is subject to change without notice.
- C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
- D. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.



DGK (S-PDSO-G8)

PLASTIC SMALL-OUTLINE PACKAGE



NOTES: A. All linear dimensions are in millimeters.

This drawing is subject to change without notice. **B.** 

Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.

- Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
- E. Falls within JEDEC MO-187 variation AA, except interlead flash.



# DGK (S-PDSO-G8)

# PLASTIC SMALL OUTLINE PACKAGE



NOTES: Α. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



 $D (R-PDSO-G14)$ 

PLASTIC SMALL OUTLINE



NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- 6 Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
- E. Reference JEDEC MS-012 variation AB.



PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



This drawing is subject to change without notice. **B.** 

 $\hat{\mathbb{C}}$  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.

 $\hat{\mathbb{D}}$  Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.

E. Falls within JEDEC MO-153



 $D (R-PDSO-G8)$ 

PLASTIC SMALL OUTLINE



NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- 6 Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
- Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
- E. Reference JEDEC MS-012 variation AA.



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