National Semiconductor

October 2007

LME49721
High Performance, High Fidelity Rail-to-Rail Input/Output Audio Operational Amplifier

General Description

The LME49721 is a low distortion, low noise Rail-to-Rail Input/Output operational amplifier optimized and fully specified for high performance, high fidelity applications. Combining advanced leading-edge process technology with state-of-the-art circuit design, the LME49721 Rail-to-Rail Input/Output operational amplifier delivers superior signal amplification for outstanding performance. The LME49721 combines a very high slew rate with low THD+N to easily satisfy demanding applications. To ensure that the most challenging loads are driven without compromise, the LME49721 has a high slew rate of ±8.5V/μs and an output current capability of ±9.7mA. Further, dynamic range is maximized by an output stage that drives 10kΩ loads to within 10mV of either power supply voltage.

The LME49721 has a wide supply range of 2.2V to 5.5V. Over this supply range the LME49721's input circuitry maintains excellent common-mode and power supply rejection, as well as maintaining its low input bias current. The LME49721 is unity gain stable.

Key Specifications

■ Power Supply Voltage Range	2.2V to 5.5V
■ Quiescent Current	2.15mA (typ)
■ THD+N ($A_V = 2$, $V_{OUT} = 4V_{p-p}$, $f_{IN} = 1kHz$)	
$R_L = 2k\Omega$	0.00008% (typ)
$R_L = 600\Omega$	0.0001% (typ)
■ Input Noise Density	$4nV/\sqrt{Hz}$ (typ), @ 1kHz
■ Slew Rate	±8.5V/μs (typ)
■ Gain Bandwidth Product	20MHz (typ)
■ Open Loop Gain ($R_L = 600\Omega$)	118dB (typ)
■ Input Bias Current	40fA (typ)
■ Input Offset Voltage	0.3mV (typ)
■ PSRR	103dB (typ)

Features

- Rail-to-rail Input and Output
- Easily drives 10kΩ loads to within 10mV of each power supply voltage
- Optimized for superior audio signal fidelity
- Output short circuit protection

Applications

- Ultra high quality portable audio amplification
- High fidelity preamplifiers
- High fidelity multimedia
- State of the art phono pre amps
- High performance professional audio
- High fidelity equalization and crossover networks
- High performance line drivers
- High performance line receivers
- High fidelity active filters
- DAC I–V converter
- ADC front-end signal conditioning

Typical Connection, Pinout, and Package Marking

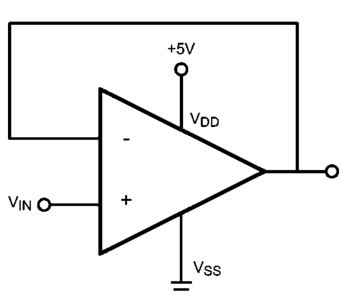
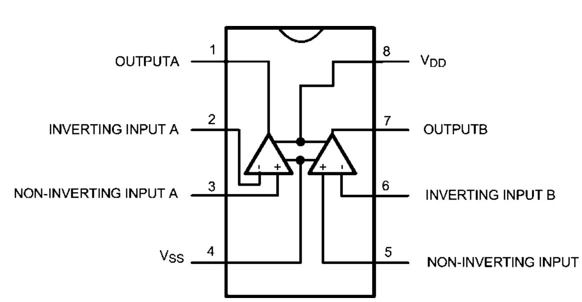
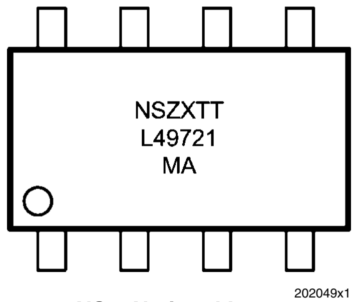


FIGURE 1. Buffer Amplifier



Order Number LME49721MA
Se NS Package Number M08A

Package Marking



NS = National Logo
Z = Assembly plant code
X = 1 Digit date code
TT = Lot traceability
L49721 = LME49721
MA = Narrow SOIC package code

Absolute Maximum Ratings (Notes 1, 2)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Power Supply Voltage ($V_S = V^+ - V^-$)	6V
Storage Temperature	−65°C to 150°C
Input Voltage	(V-) - 0.7V to (V+) + 0.7V
Output Short Circuit (Note 3)	Continuous
Power Dissipation	Internally Limited
ESD Rating (Note 4)	2000V
ESD Rating (Note 5)	200V
Junction Temperature	150°C
Thermal Resistance	
θ_{JA} (SO)	165°C/W
Temperature Range	
$T_{MIN} \le T_A \le T_{MAX}$	$-40°C \le T_A \le 85°C$
Supply Voltage Range	$2.2V \le V_S \le 5.5V$

Electrical Characteristics for the LME49721

The following specifications apply for the circuit shown in Figure 1. V_S = 5V, R_L = 10kΩ, R_{SOURCE} = 10Ω, f_{IN} = 1kHz, and T_A = 25°C, unless otherwise specified.

Symbol	Parameter	Conditions	LME49721 Typical (Note 6)	LME49721 Limit (Note 7)	Units (Limits)
THD+N	Total Harmonic Distortion + Noise	A_V = +1, V_{OUT} = $2V_{p-p}$, R_L = 2kΩ	0.0002		
		R_L = 600Ω	0.0002	0.001	% (max)
IMD	Intermodulation Distortion	A_V = +1, V_{OUT} = $2V_{p-p}$, Two-tone, 60Hz & 7kHz 4:1	0.0004		%
GBWP	Gain Bandwidth Product		20	15	MHz (min)
SR	Slew Rate	A_V = +1	8.5		V/μs (min)
FPBW	Full Power Bandwidth	V_{OUT} = $1V_{P-P}$, –3dB referenced to output magnitude at f = 1kHz	2.2		MHz
t_s	Settling time	A_V = 1, 4V step 0.1% error range	800		ns
e_n	Equivalent Input Noise Voltage	f_{BW} = 20Hz to 20kHz, A-weighted	.707	1.13	μV_{P-P} (max)
	Equivalent Input Noise Density	f = 1kHz A-weighted	4	6	$nV/\sqrt{Hz}$ (max)
i_n	Current Noise Density	f = 10kHz	4.0		$fA/\sqrt{Hz}$
V_{OS}	Offset Voltage		0.3	1.5	mV (max)
$\Delta V_{OS}/\Delta Temp$	Average Input Offset Voltage Drift vs Temperature	$40°C \le T_A \le 85°C$	1.1		μV/°C
PSRR	Average Input Offset Voltage Shift vs Power Supply Voltage		103	85	dB (min)
ISO_{CH-CH}	Channel-to-Channel Isolation	f_{IN} = 1kHz	117		dB
I_B	Input Bias Current	$V_{CM} = V_S/2$	40		fA
$\Delta I_{OS}/\Delta Temp$	Input Bias Current Drift vs Temperature	$-40°C \le T_A \le 85°C$	48		fA/°C
I_{OS}	Input Offset Current	$V_{CM} = V_S/2$	60		fA
V_{IN-CM}	Common-Mode Input Voltage Range			(V+) – 0.1 (V-) + 0.1	V (min)
CMRR	Common-Mode Rejection	V_{SS} - 100mV < V_{CM} < V_{DD} + 100mV	93	70	dB (min)
	1/f Corner Frequency		2000		Hz
A_{VOL}	Open Loop Voltage Gain	V_{SS} - 200mV < V_{OUT} < V_{DD} + 200mV			
		R_L = 600Ω	118	100	dB (min)
		R_L = 2kΩ	122		dB (min)
		R_L = 10kΩ	130	115	dB (min)

Symbol	Parameter	Conditions	LME49721		Units (Limits)
			Typical	Limit	
			(Note 6)	(Note 7)	
V_{OUTMIN}	Output Voltage Swing	R_L = 600Ω	V_{DD} – 30mV	V_{DD} – 80mV	V (min)
			V_{SS} + 30mV	V_{SS} + 80mV	V (min)
		R_L = 10kΩ, V_S = 5.0V	V_{DD} – 10mV	V_{DD} – 20mV	V (min)
			V_{SS} + 10mV	V_{SS} + 20mV	V (min)
I_{OUT}	Output Current	R_L = 250Ω, V_S = 5.0V	9.7	9.3	mA (min)
I_{OUT-SC}	Short Circuit Current		100		mA
R_{OUT}	Output Impedance	f_{IN} = 10kHz Closed-Loop Open-Loop	 0.01 46		Ω
I_S	Quiescent Current per Amplifier	I_{OUT} = 0mA	2.15	3.25	mA (max)

Note 1: "*Absolute Maximum Ratings*" indicate limits beyond which damage to the device may occur, including inoperability and degradation of device reliability and/or performance. Functional operation of the device and/or non-degradation at the *Absolute Maximum Ratings* or other conditions beyond those indicated in the Recommended Operating Conditions is not implied. The *Recommended Operating Conditions* indicate conditions at which the device is functional and the device should not be operated beyond such conditions. All voltages are measured with respect to the ground pin, unless otherwise specified

Note 2: The *Electrical Characteristics* tables list guaranteed specifications under the listed *Recommended Operating Conditions* except as otherwise modified or specified by the *Electrical Characteristics Conditions* and/or Notes. Typical specifications are estimations only and are not guaranteed.

Note 3: The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{JMAX}, θ_{JA}, and the ambient temperature, T_A. The maximum allowable power dissipation is $P_{DMAX} = (T_{JMAX} - T_A) / \theta_{JA}$ or the number given in *Absolute Maximum Ratings*, whichever is lower.

Note 4: Human body model, applicable std. JESD22-A114C.

Note 5: Machine model, applicable std. JESD22-A115-A.

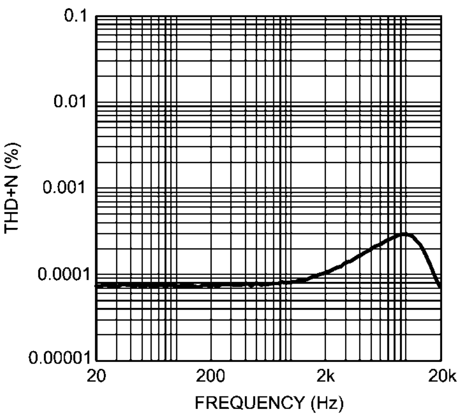
Note 6: Typical values represent most likely parametric norms at T_A = +25ºC, and at the *Recommended Operation Conditions* at the time of product characterization and are not guaranteed.

Note 7: Datasheet min/max specification limits are guaranteed by test or statistical analysis.

Typical Performance Characteristics

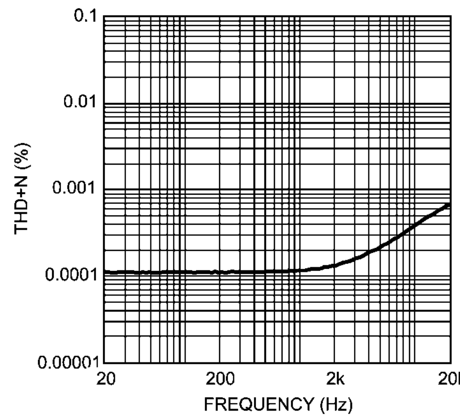
Graphs were taken in dual supply configuration.

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 2kΩ, A_V = 2, BW = 22kHz



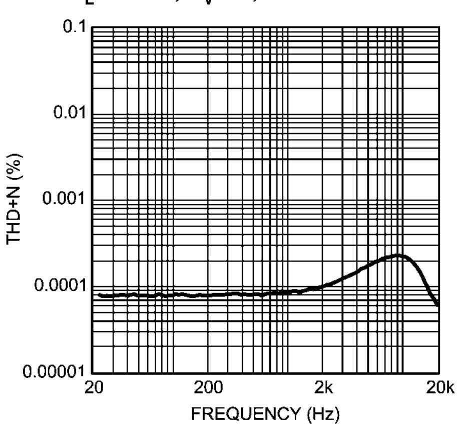
202049t6

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 2kΩ, A_V = 2



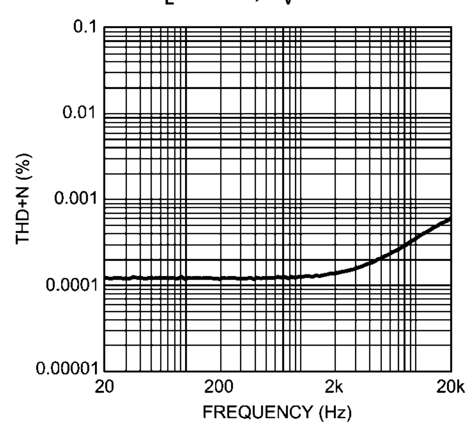
202049t5

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 10kΩ, A_V = 2, BW = 22kHz



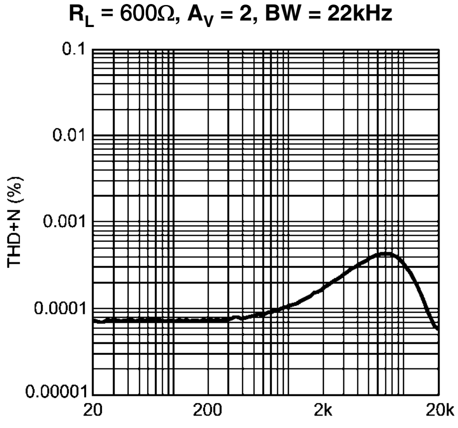
202049t8

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 10kΩ, A_V = 2



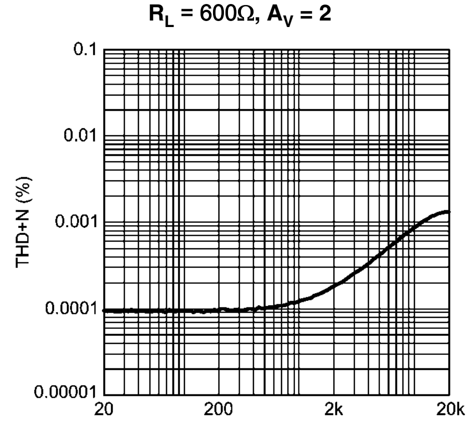
202049t7

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 600Ω, A_V = 2, BW = 22kHz



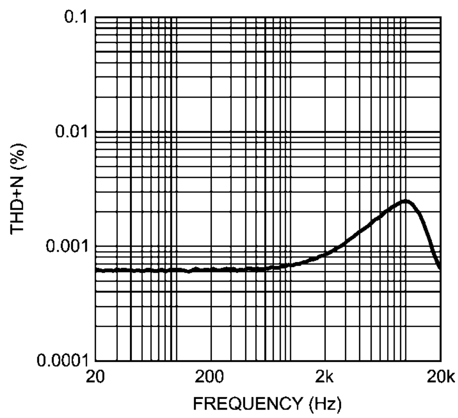
202049u0

THD+N vs Frequency
V_S = ±2.5V, V_{OUT} = $4V_{P-P}$
R_L = 600Ω, A_V = 2



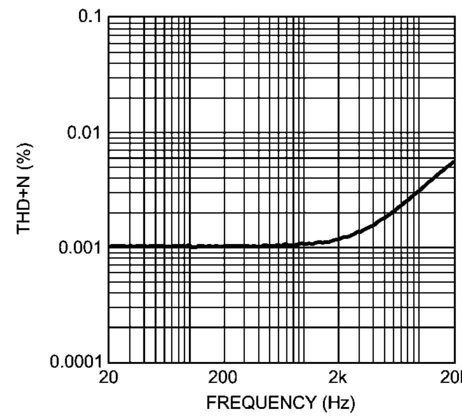
202049t9

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 2kΩ, A_V = 2, BW = 22kHz



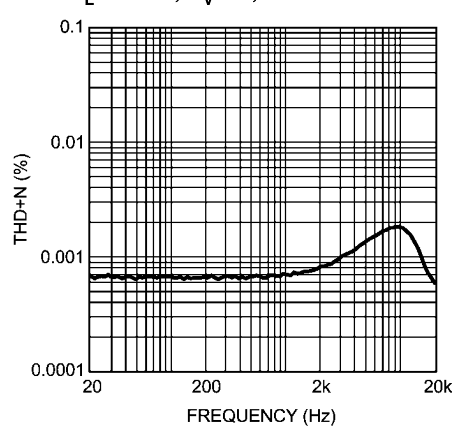
202049u2

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 2kΩ, A_V = 2



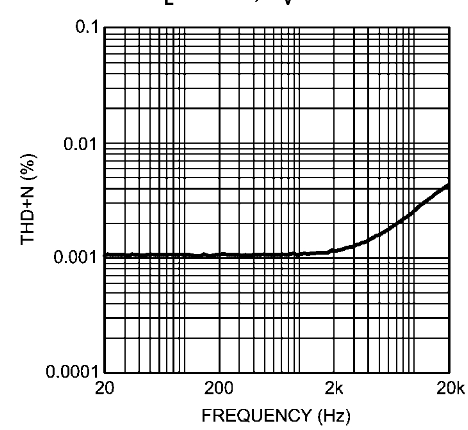
202049u1

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 10kΩ, A_V = 2, BW = 22kHz



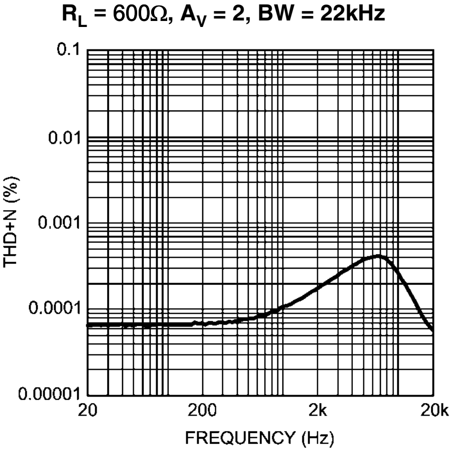
202049u4

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 10kΩ, A_V = 2



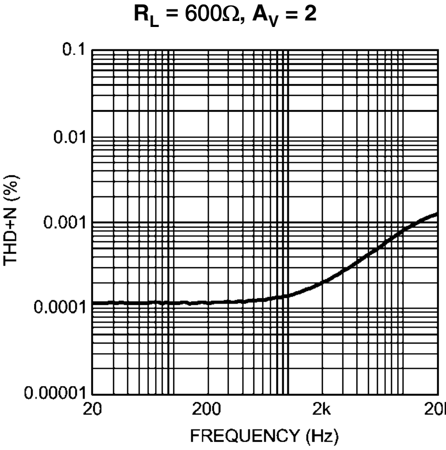
202049u3

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 600Ω, A_V = 2, BW = 22kHz



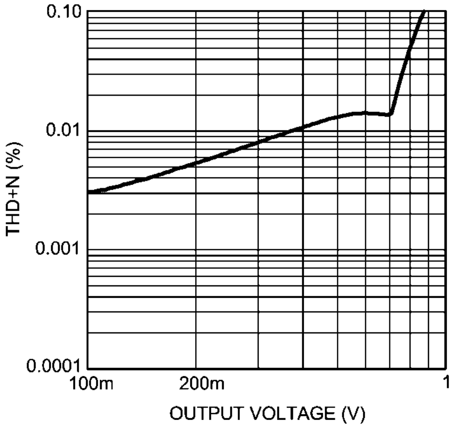
202049u5

THD+N vs Frequency
V_S = ±2.75V, V_{OUT} = $4V_{P-P}$
R_L = 600Ω, A_V = 2



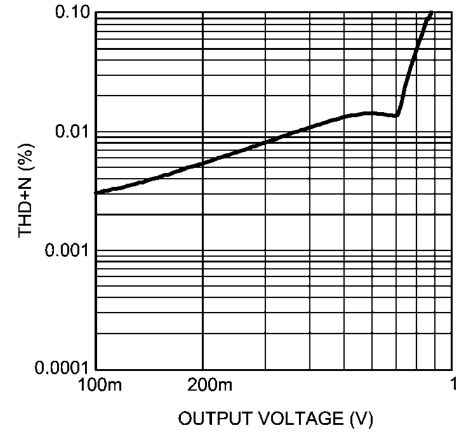
202049u6

THD+N vs Output Voltage
$V_S = \pm1.1V$
$R_L = 2k\Omega, A_V = 2$



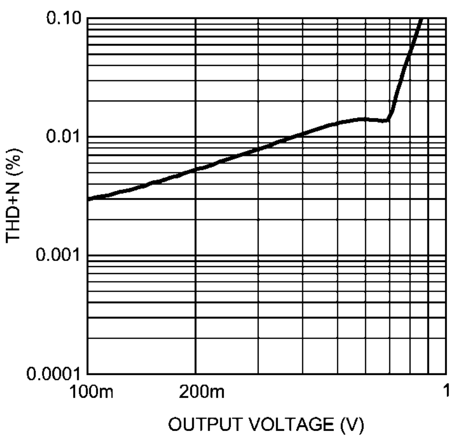
202049u7

THD+N vs Output Voltage
$V_S = \pm1.1V$
$R_L = 10k\Omega, A_V = 2$



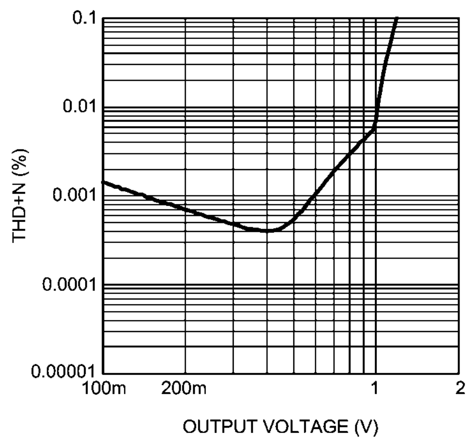
202049u8

THD+N vs Output Voltage
$V_S = \pm1.1V$
$R_L = 600\Omega, A_V = 2$



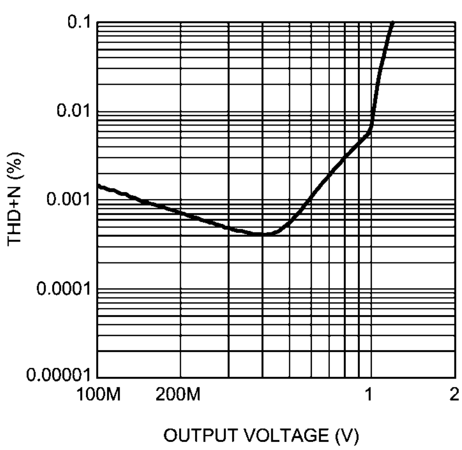
202049u9

THD+N vs Output Voltage
$V_S = \pm1.5V$
$R_L = 2k\Omega, A_V = 2$



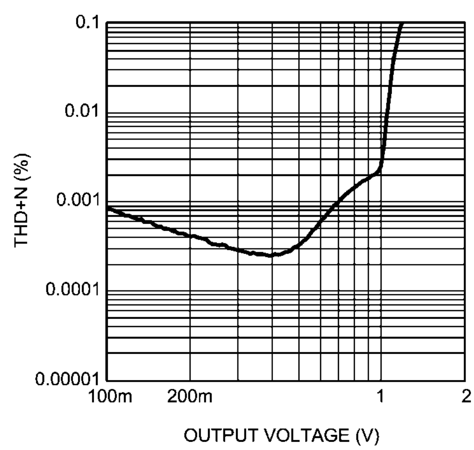
202049v0

THD+N vs Output Voltage
$V_S = \pm1.5V$
$R_L = 10k\Omega, A_V = 2$



202049v1

THD+N vs Output Voltage
$V_S = \pm1.5V$
$R_L = 600\Omega, A_V = 2$



202049v2

THD+N vs Output Voltage
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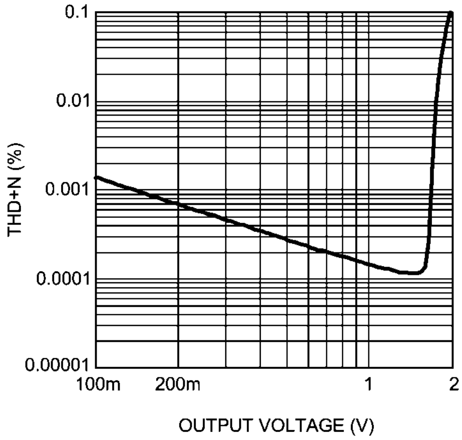
$R_L = 2k\Omega$, $A_V = 2$



202049v3

THD+N vs Output Voltage
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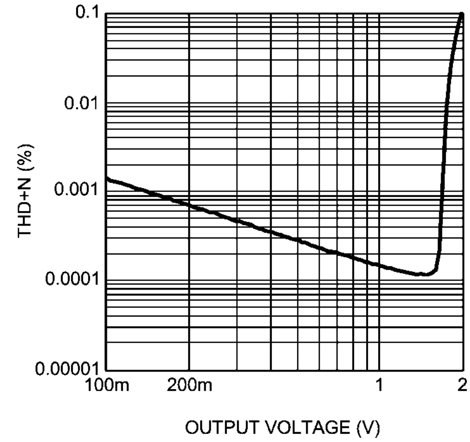

202049v4

THD+N vs Output Voltage
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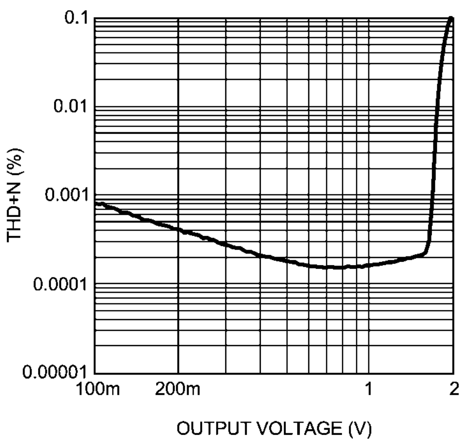
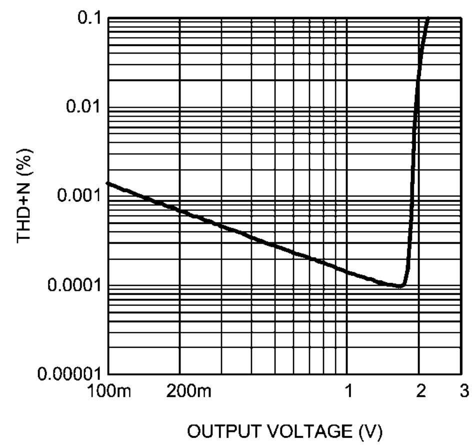


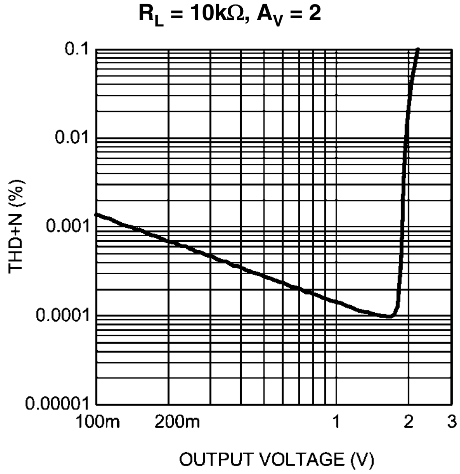
202049v5

THD+N vs Output Voltage
$V_S = \pm2.75V$
$R_L = 2k\Omega$, $A_V = 2$



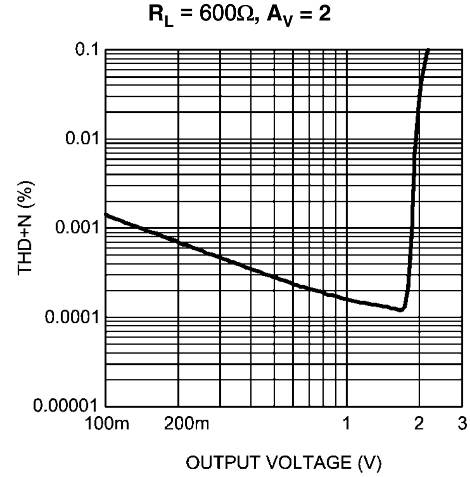
202049v6

THD+N vs Output Voltage
$V_S = \pm2.75V$
$R_L = 10k\Omega$, $A_V = 2$



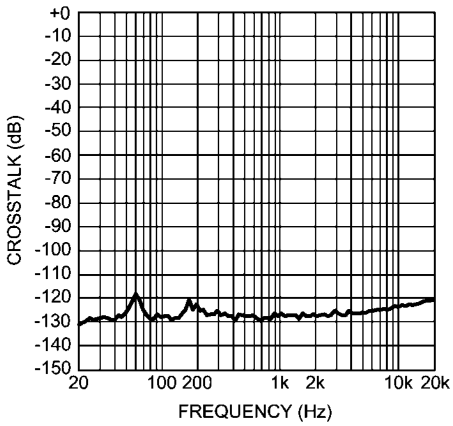
202049v7

THD+N vs Output Voltage
$V_S = \pm2.75V$
$R_L = 600\Omega$, $A_V = 2$



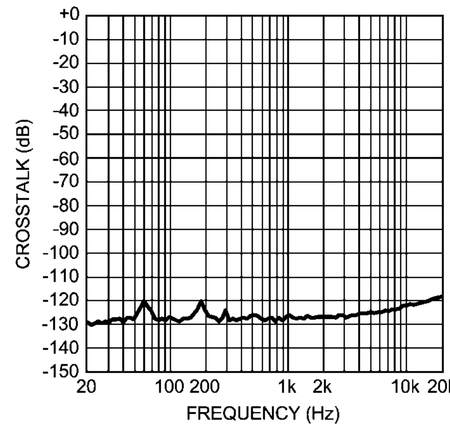
202049v8

Crosstalk vs Frequency
V_S = ±1.1V
V_{OUT} = 2V_{p-p}
R_L = 2kΩ



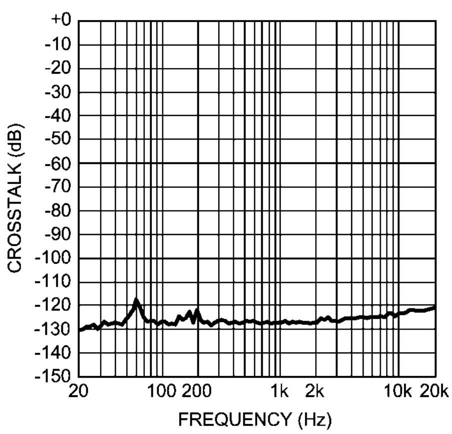
202049r4

Crosstalk vs Frequency
V_S = ±1.1V
V_{OUT} = 2V_{p-p}
R_L = 10kΩ



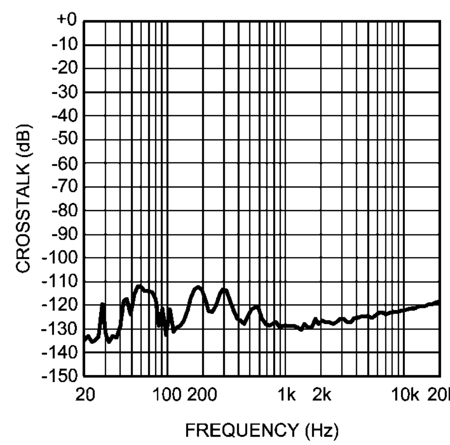
202049r5

Crosstalk vs Frequency
V_S = ±1.1V
V_{OUT} = 2V_{p-p}
R_L = 600Ω



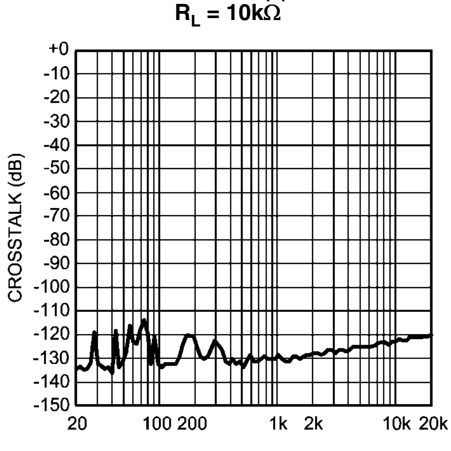
202049r6

Crosstalk vs Frequency
V_S = ±1.5V,
V_{OUT} = 2V_{p-p}
R_L = 2kΩ



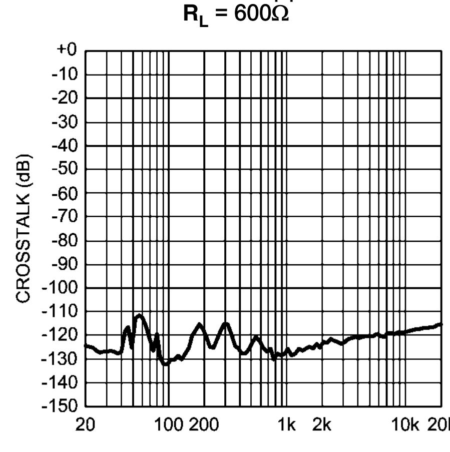
202049k1

Crosstalk vs Frequency
V_S = ±1.5V
V_{OUT} = 2V_{p-p}
R_L = 10kΩ



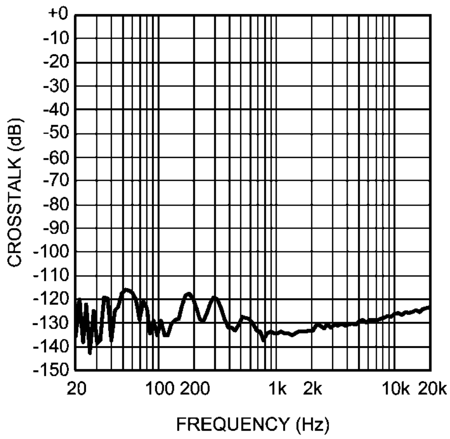
202049k2

Crosstalk vs Frequency
V_S = ±1.5V
V_{OUT} = 2V_{p-p}
R_L = 600Ω



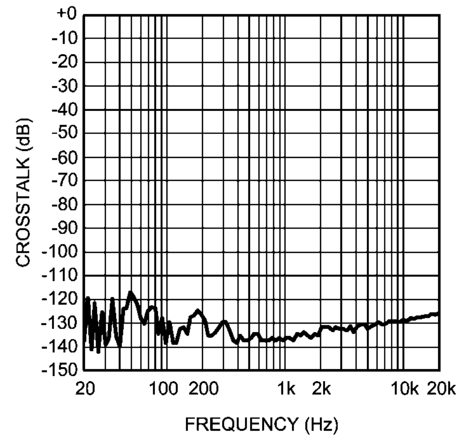
202049k3

Crosstalk vs Frequency
$V_S = \pm 2.5V$
$V_{OUT} = 4V_{p-p}$
$R_L = 2k\Omega$



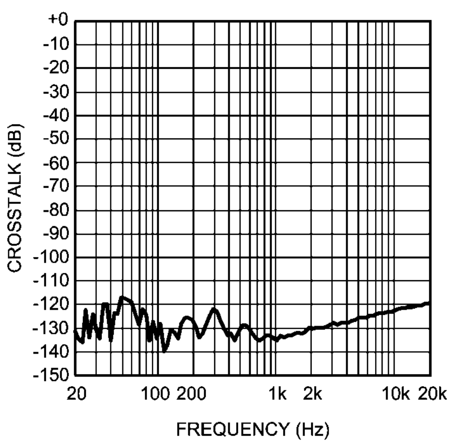
202049k4

Crosstalk vs Frequency
$V_S = \pm 2.5V$
$V_{OUT} = 4V_{p-p}$
$R_L = 10k\Omega$



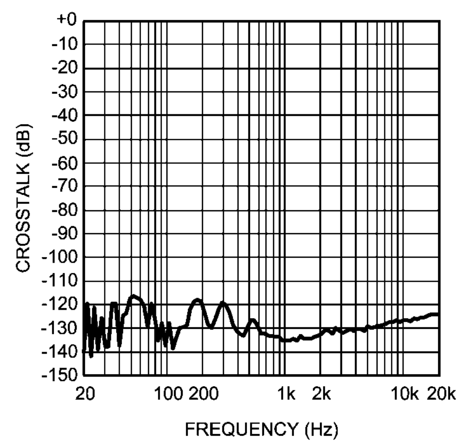
202049k5

Crosstalk vs Frequency
$V_S = \pm 2.5V$
$V_{OUT} = 4V_{p-p}$
$R_L = 600\Omega$



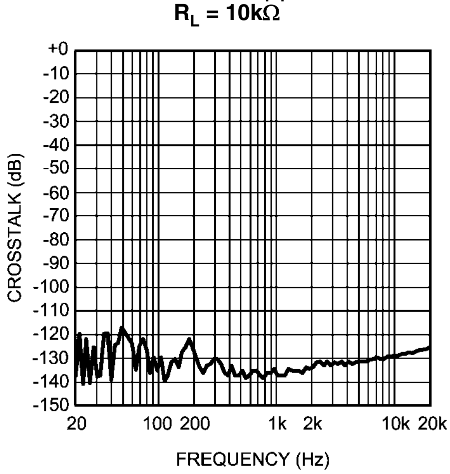
202049k6

Crosstalk vs Frequency
$V_S = \pm 2.75V$
$V_{OUT} = 4V_{p-p}$
$R_L = 2k\Omega$



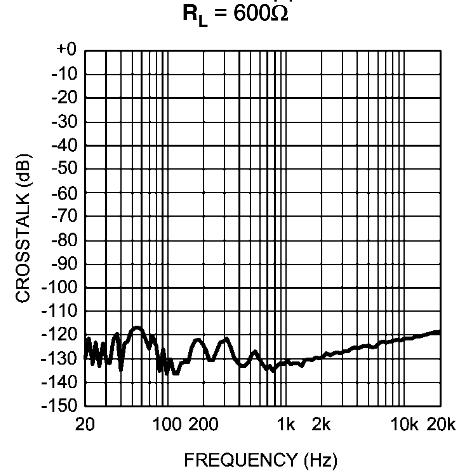
202049k7

Crosstalk vs Frequency
$V_S = \pm 2.75V$
$V_{OUT} = 4V_{p-p}$
$R_L = 10k\Omega$



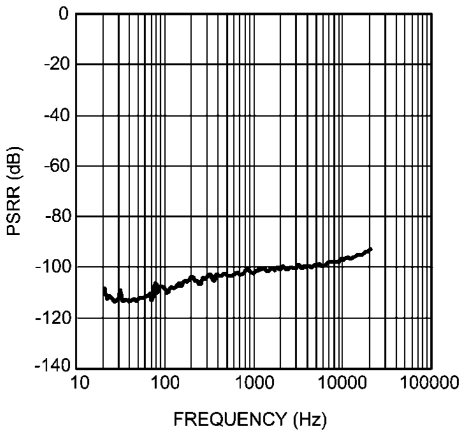
202049k8

Crosstalk vs Frequency
$V_S = \pm 2.75V$
$V_{OUT} = 4V_{p-p}$
$R_L = 600\Omega$



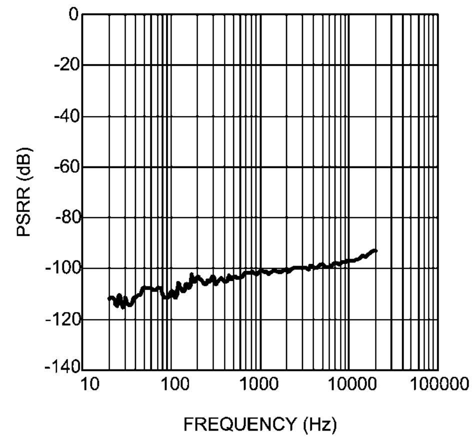
202049k9

PSRR vs Frequency
V_S = ±1.1V
V_{RIPPLE} = 200mV_{P-P}
R_L = 2kΩ



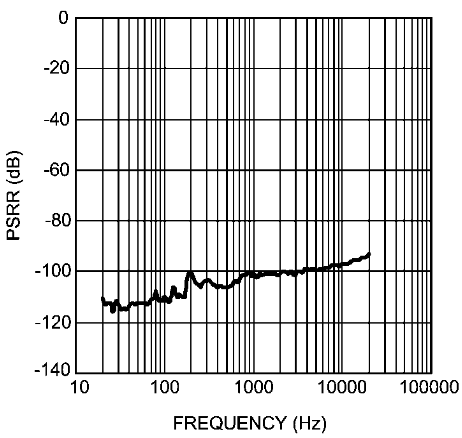
202049v9

PSRR vs Frequency
V_S = ±1.1V
V_{RIPPLE} = 200mV_{P-P}
R_L = 10kΩ



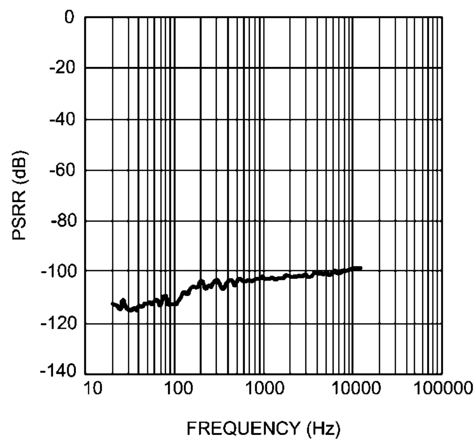
202049w0

PSRR vs Frequency
V_S = ±1.1V
V_{RIPPLE} = 200mV_{P-P}
R_L = 600Ω



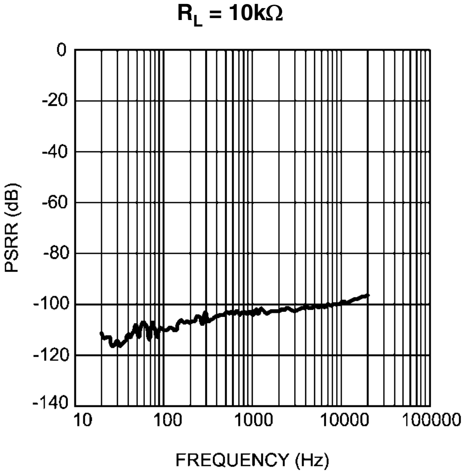
202049w1

PSRR vs Frequency
V_S = ±1.5V
V_{RIPPLE} = 200mV_{P-P}
R_L = 2kΩ



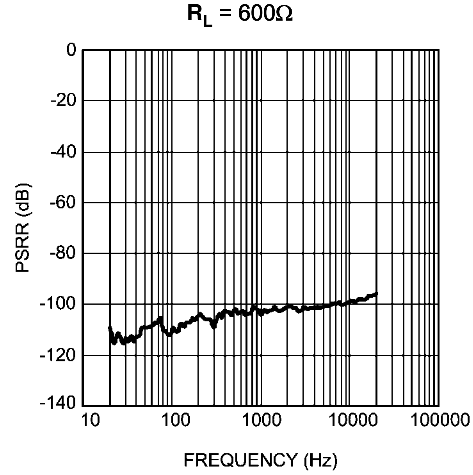
202049w2

PSRR vs Frequency
V_S = ±1.5V
V_{RIPPLE} = 200mV_{P-P}
R_L = 10kΩ



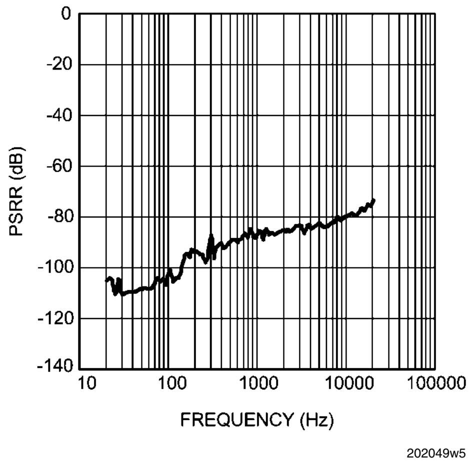
202049w3

PSRR vs Frequency
V_S = ±1.5V
V_{RIPPLE} = 200mV_{P-P}
R_L = 600Ω

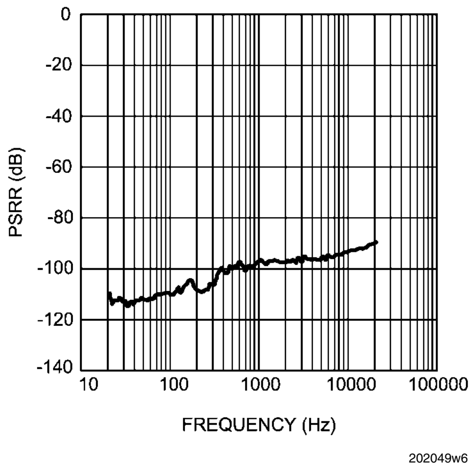


202049x4

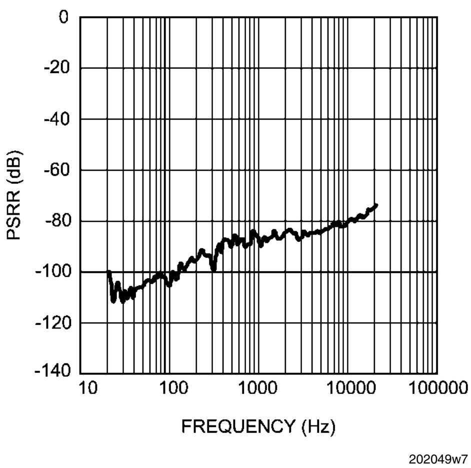
PSRR vs Frequency
V_S = ±2.5V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 2kΩ



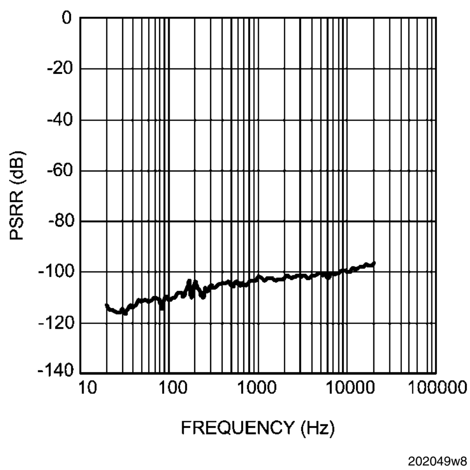
PSRR vs Frequency
V_S = ±2.5V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 10kΩ



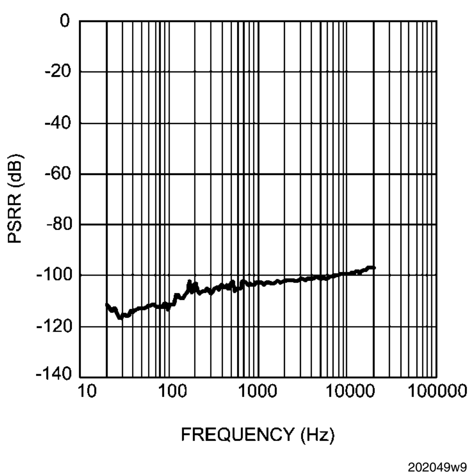
PSRR vs Frequency
V_S = ±2.5V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 600Ω



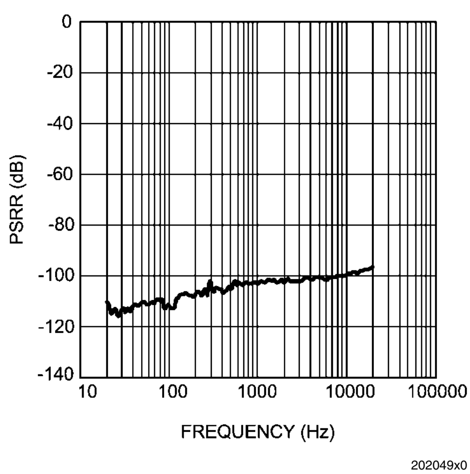
PSRR vs Frequency
V_S = ±2.75V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 2kΩ



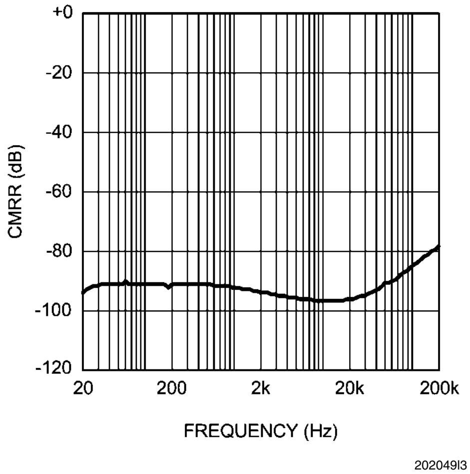
PSRR vs Frequency
V_S = ±2.75V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 10kΩ



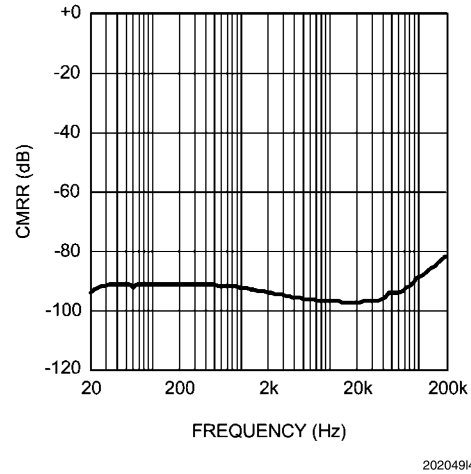
PSRR vs Frequency
V_S = ±2.75V
V_{RIPPLE} = 200mV$_{P-P}$
R_L = 600Ω



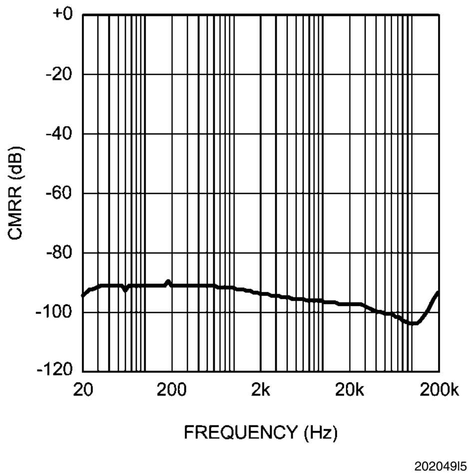
CMRR vs Frequency
V_S = ±1.5V
R_L = 2kΩ



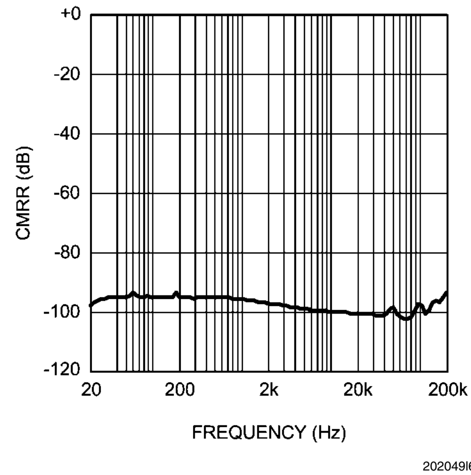
CMRR vs Frequency
V_S = ±1.5V
R_L = 10kΩ



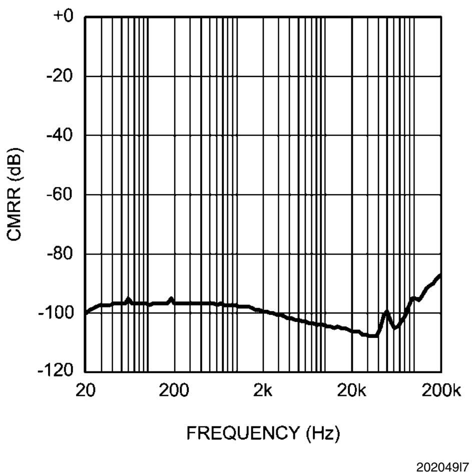
CMRR vs Frequency
V_S = ±1.5V
R_L = 600Ω



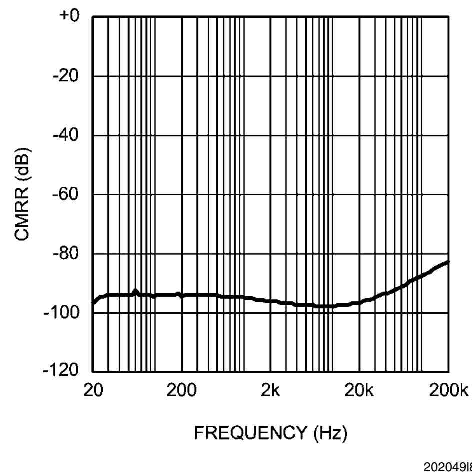
CMRR vs Frequency
V_S = ±2.5V
R_L = 2kΩ



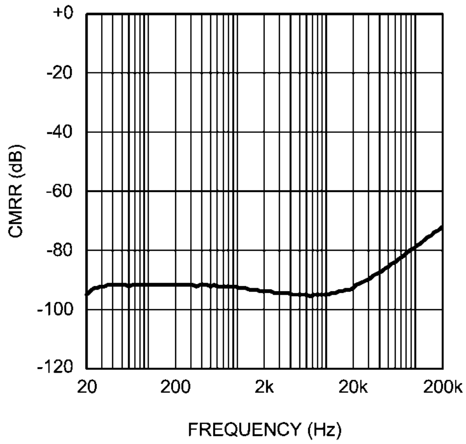
CMRR vs Frequency
V_S = ±2.5V
R_L = 10kΩ



CMRR vs Frequency
V_S = ±2.5V
R_L = 600Ω

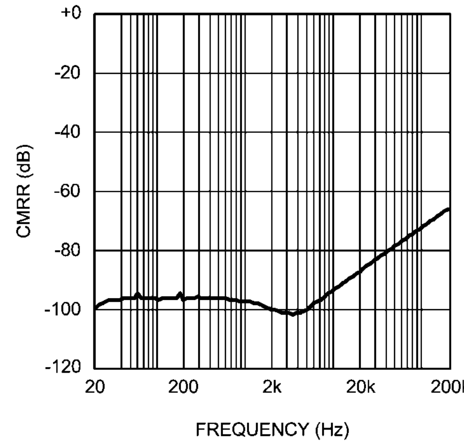


CMRR vs Frequency
$V_S = \pm 2.75V$
$R_L = 2k\Omega$



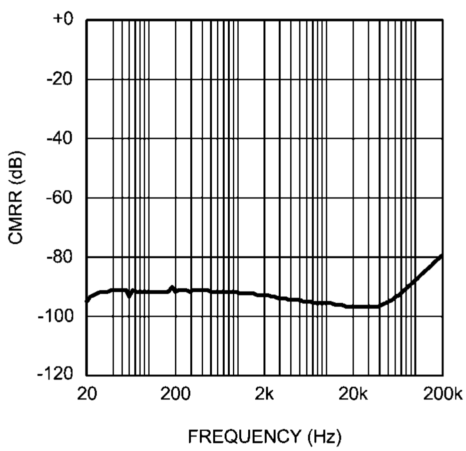
202049l9

CMRR vs Frequency
$V_S = \pm 2.75V$
$R_L = 10k\Omega$



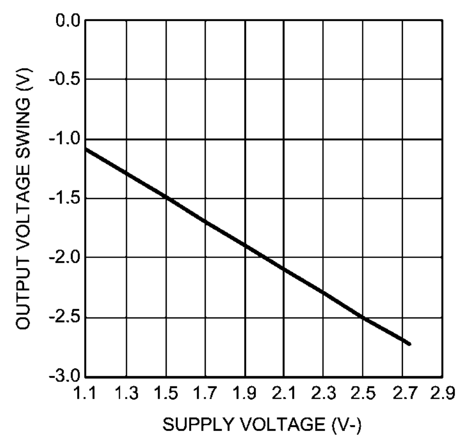
202049m0

CMRR vs Frequency
$V_S = \pm 2.75V$
$R_L = 600\Omega$



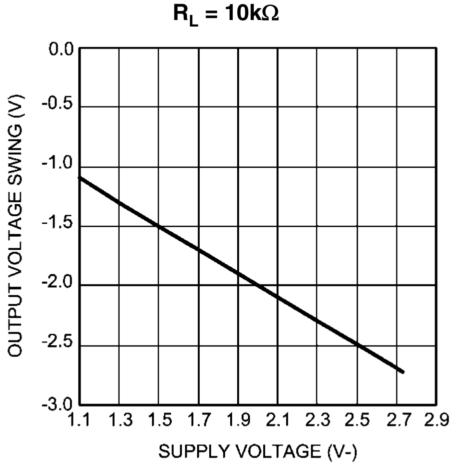
202049m1

Output Voltage Swing Neg vs Power Supply
$R_L = 2k\Omega$



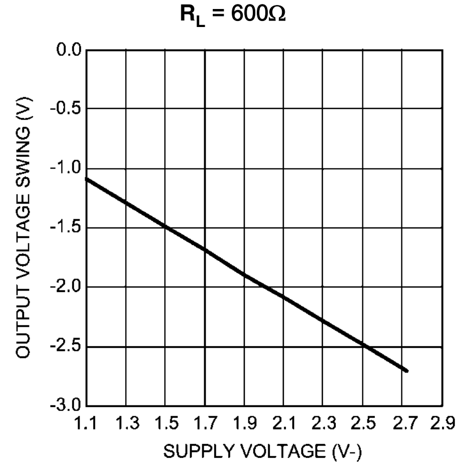
202049s9

Output Voltage Swing Neg vs Power Supply
$R_L = 10k\Omega$



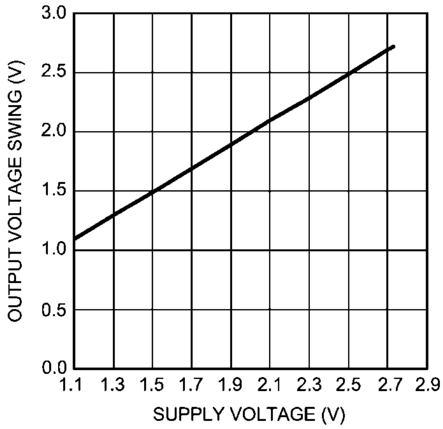
202049t0

Output Voltage Swing Neg vs Power Supply
$R_L = 600\Omega$



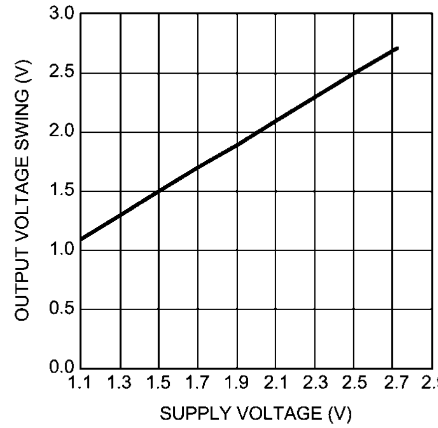
202049t1

Output Voltage Swing Pos vs Power Supply
R_L = 2kΩ



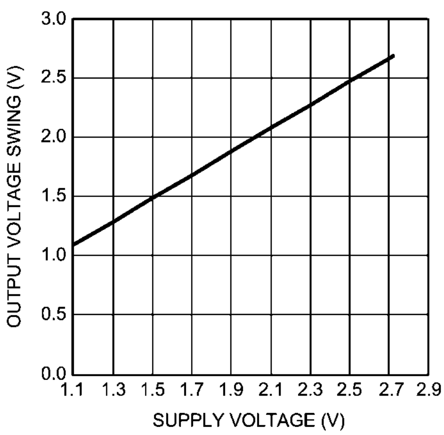
202049t2

Output Voltage Swing Pos vs Power Supply
R_L = 10kΩ



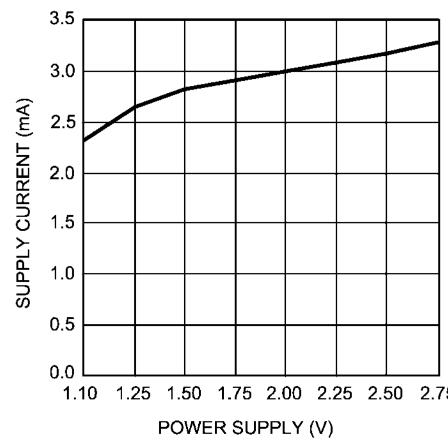
202049t3

Output Voltage Swing Pos vs Power Supply
R_L = 600Ω



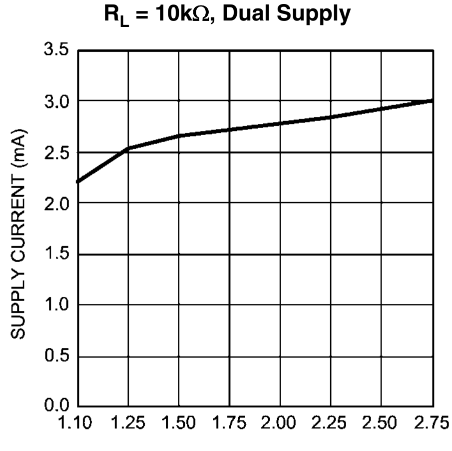
202049t4

Supply Current per amplifier vs Power Supply
R_L = 2kΩ, Dual Supply



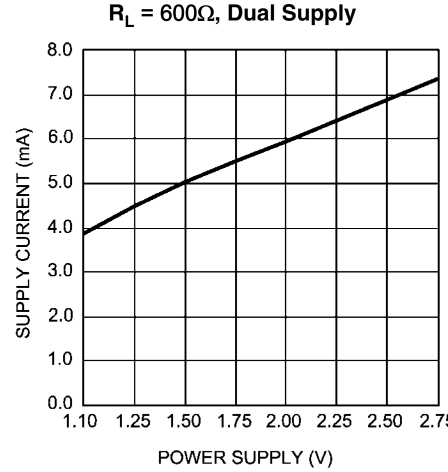
20204953

Supply Current per amplifier vs Power Supply
R_L = 10kΩ, Dual Supply



20204954

Supply Current per amplifier vs Power Supply
R_L = 600Ω, Dual Supply



20204956

Application Information

DISTORTION MEASUREMENTS

The vanishingly low residual distortion produced by LME49721 is below the capabilities of all commercially available equipment. This makes distortion measurements just slightly more difficult than simply connecting a distortion meter to the amplifier's inputs and outputs. The solution. however, is quite simple: an additional resistor. Adding this resistor extends the resolution of the distortion measurement equipment.

The LME49721's low residual is an input referred internal error. As shown in Figure 1, adding the 10Ω resistor connected between athe amplifier's inverting and non-inverting inputs changes the amplifier's noise gain. The result is that the error signal (distortion) is amplified by a factor of 101. Although the amplifier's closed-loop gain is unaltered, the feedback available to correct distortion errors is reduced by 101. To ensure minimum effects on distortion measurements, keep the value of R1 low as shown in Figure 1.

This technique is verified by duplicating the measurements with high closed loop gain and/or making the measurements at high frequencies. Doing so, produces distortion components that are within equipments capabilities. This datasheet's THD+N and IMD values were generated using the above described circuit connected to an Audio Precision System Two Cascade.

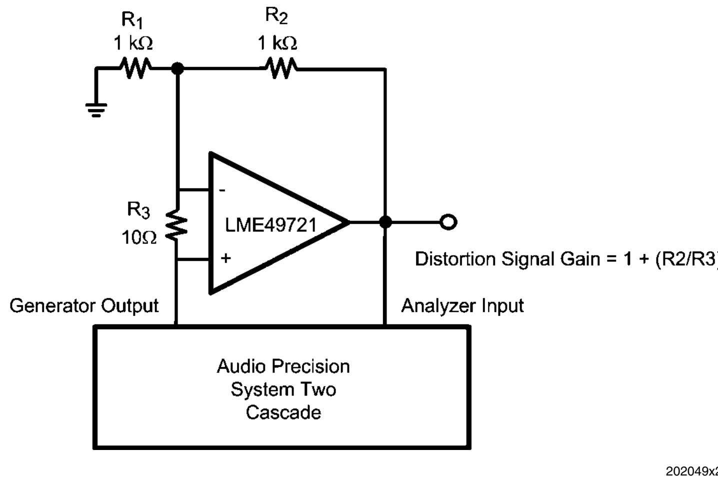


FIGURE 1. THD+N and IMD Distortion Test Circuit with A_V = 2

OPERATING RATINGS AND BASIC DESIGN GUIDELINES

The LME49721 has a supply voltage range from +2.2V to +5.5V single supply or ±1.1 to ±2.75V dual supply.

Bypassed capacitors for the supplies should be placed as close to the amplifier as possible. This will help minimize any inductance between the power supply and the supply pins. In addition to a 10µF capacitor, a 0.1µF capacitor is also recommended in CMOS amplifiers.

The amplifier's inputs lead lengths should also be as short as possible. If the op amp does not have a bypass capacitor, it may oscillate.

BASIC AMPLIFIER CONFIGURATIONS

The LME49721 may be operated with either a single supply or dual supplies. Figure 2 shows the typical connection for a single supply inverting amplifier. The output voltage for a single supply amplifier will be centered around the common-mode voltage Vcm. Note, the voltage applied to the Vcm insures the output stays above ground. Typically, the Vcm should be equal to $V_{DD}/2$. This is done by putting a resistor divider ckt at this node, see Figure 2.

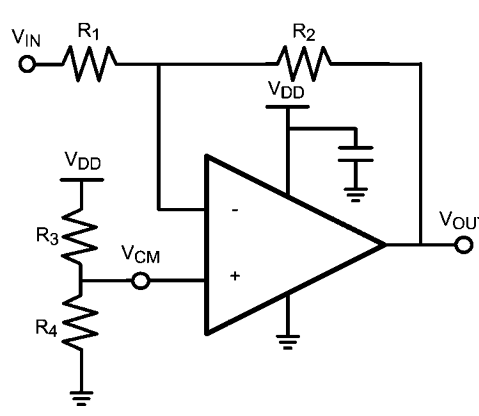


FIGURE 2. Single Supply Inverting Op Amp

Figure 3 shows the typical connection for a dual supply inverting amplifier. The output voltage is centered on zero.

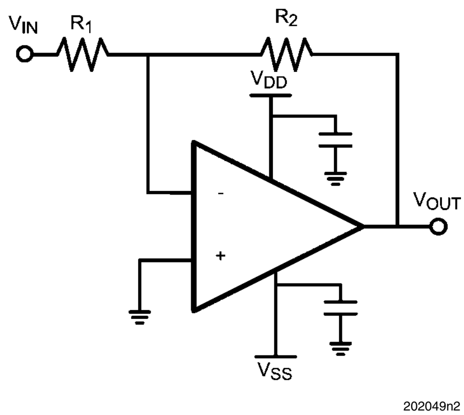


FIGURE 3. Dual Supply Inverting Op Amp

Figure 4 shows the typical connection for the Buffer Amplifier or also called a Voltage Follower. A Buffer Amplifier can be used to solve impedance matching problems, to reduce power consumption in the source, or to drive heavy loads. The input impedance of the op amp is very high. Therefore, the input of the op amp does not load down the source. The output impedance on the other hand is very low. It allows the load to either supply or absorb energy to a circuit while a secondary voltage source dissipates energy from a circuit. The Buffer is a unity stable amplifier, 1V/V. Although the feedback loop is tied from the output of the amplifier to the inverting input, the gain is still positive. Note, if a positive feedback is used, the amplifier will most likely drive to either rail at the output.

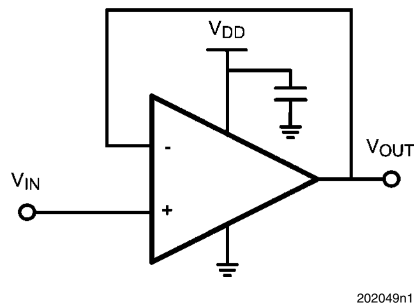
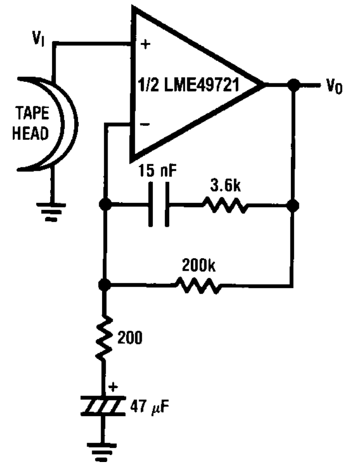


FIGURE 4. Buffer

Typical Applications

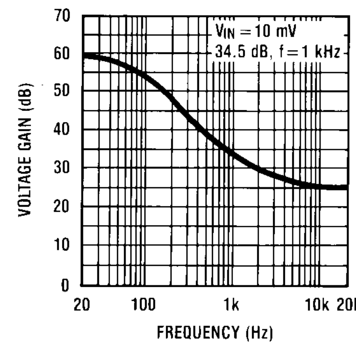
ANAB Preamp



202049n4

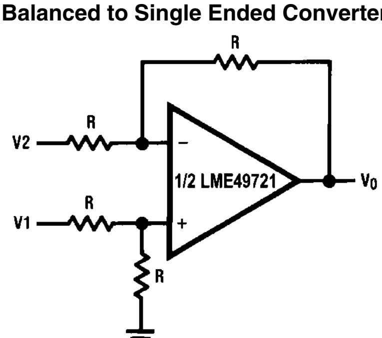
$A_V = 34.5$
F = 1 kHz
$E_n = 0.38\ \mu V$
A Weighted

NAB Preamp Voltage Gain vs Frequency



202049n5

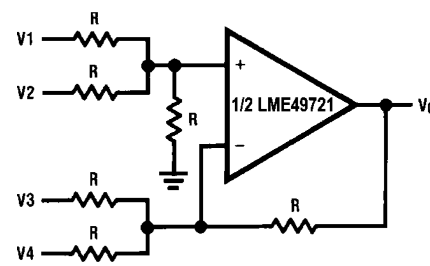
Balanced to Single Ended Converter



202049n6

$V_O = V1 - V2$

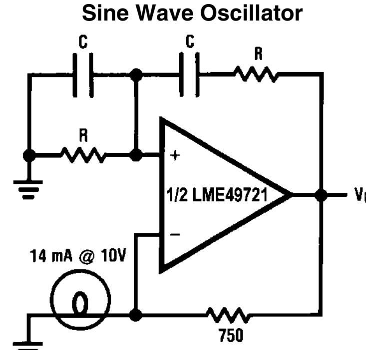
Adder/Subtracter



202049n7

$V_O = V1 + V2 - V3 - V4$

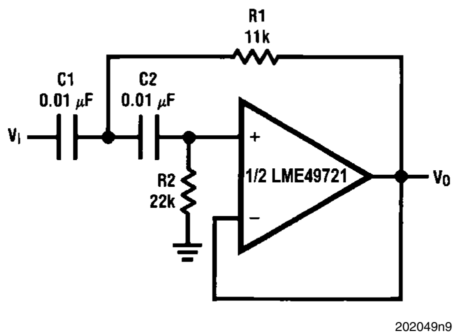
Sine Wave Oscillator



202049n8

$$f_O = \frac{1}{2\pi RC}$$

Second Order High Pass Filter (Butterworth)



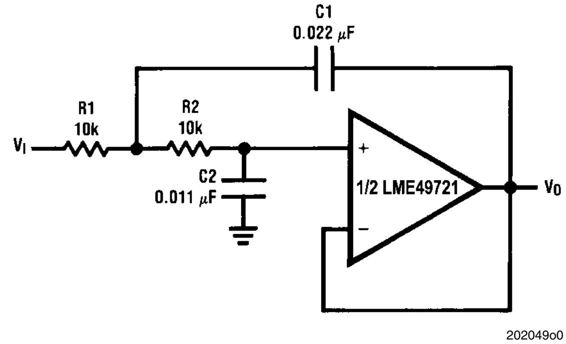
if C1 = C2 = C

$$R1 = \frac{\sqrt{2}}{2\omega_o C}$$

$$R2 = 2 \bullet R1$$

Illustration is f_0 = 1 kHz

Second Order Low Pass Filter (Butterworth)



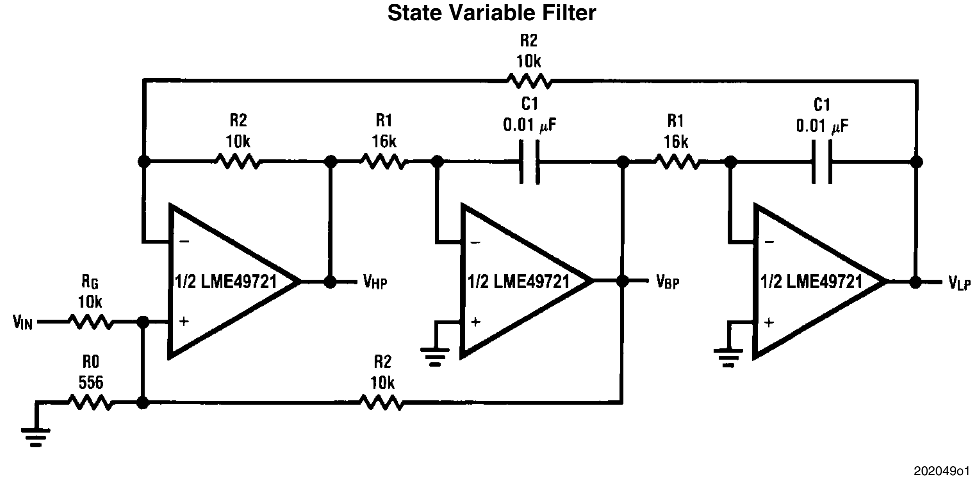
if R1 = R2 = R

$$C1 = \frac{\sqrt{2}}{\omega_o R}$$

$$C2 = \frac{C1}{2}$$

Illustration is f_0 = 1 kHz

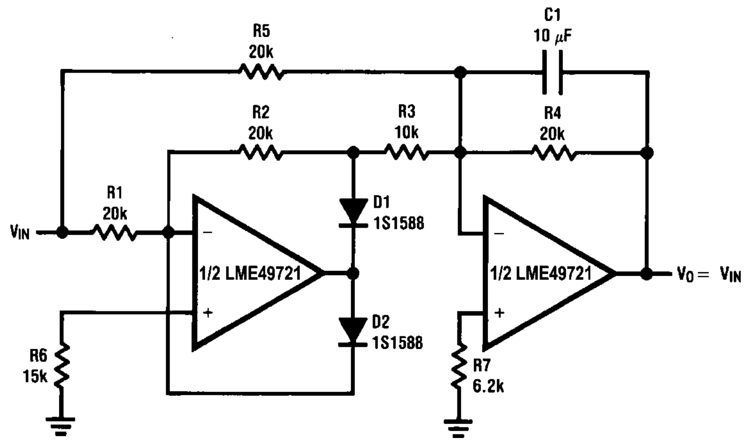
State Variable Filter



$$f_0 = \frac{1}{2\pi C1R1}, Q = \frac{1}{2}\left(1 + \frac{R2}{R0} + \frac{R2}{RG}\right), A_{BP} = QA_{LP} = QA_{LH} = \frac{R2}{RG}$$

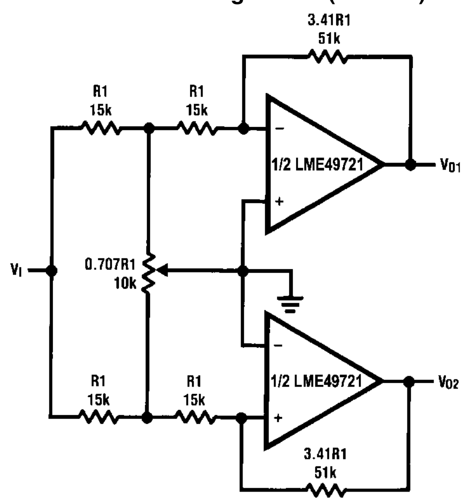
Illustration is f_0 = 1 kHz, Q = 10, A_{BP} = 1

AC/DC Converter



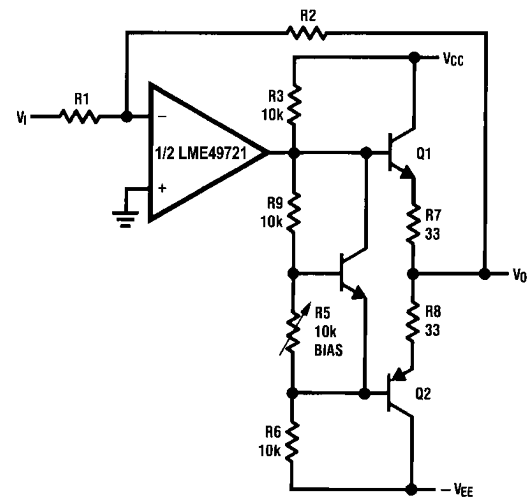
20204902

2 Channel Panning Circuit (Pan Pot)



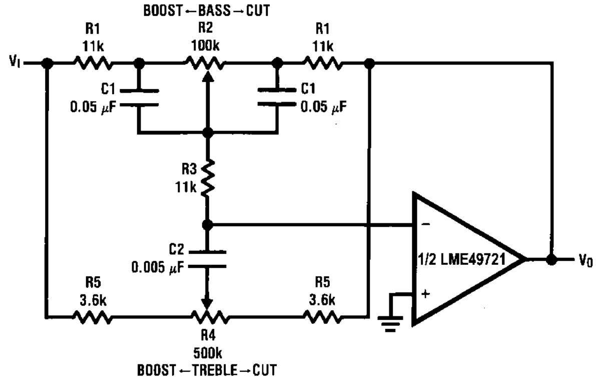
20204903

Line Driver



20204904

Tone Control



20204905

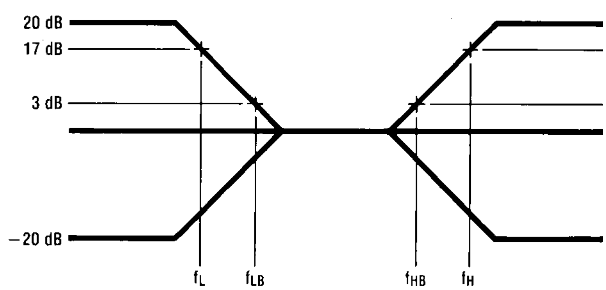
$$f_L = \frac{1}{2\pi R2C1}, f_{LB} = \frac{1}{2\pi R1C1}$$

$$f_H = \frac{1}{2\pi R5C2}, f_{HB} = \frac{1}{2\pi (R1 + R5 + 2R3)C2}$$

Illustration is:

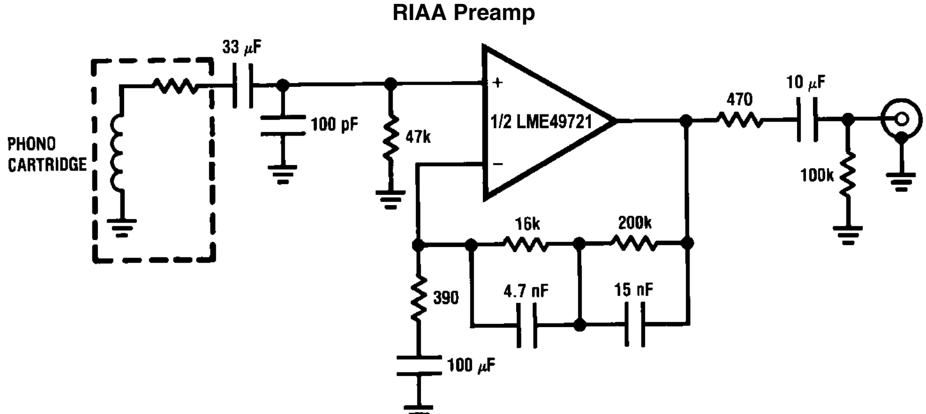
f_L = 32 Hz, f_{LB} = 320 Hz

f_H =11 kHz, f_{HB} = 1.1 kHz



20204906

RIAA Preamp



20204908

A_v = 35 dB

E_n = 0.33 μV

S/N = 90 dB

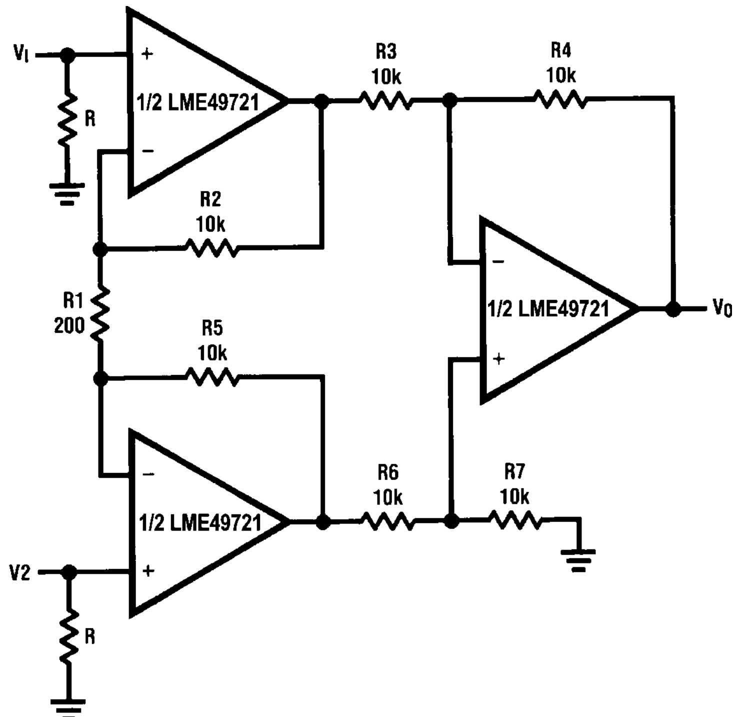
f = 1 kHz

A Weighted

A Weighted, V_{IN} = 10 mV

@f = 1 kHz

Balanced Input Mic Amp



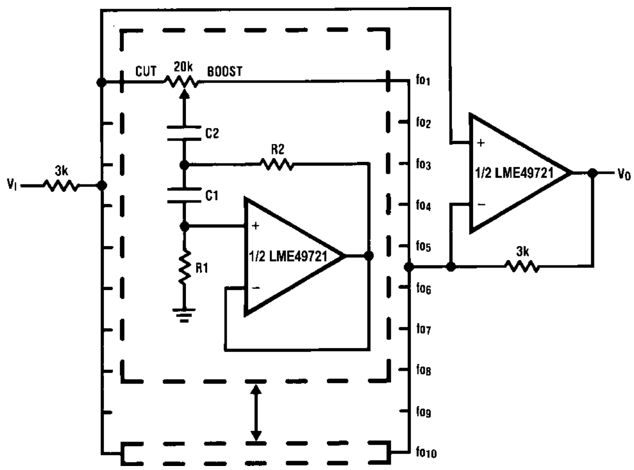
If R2 = R5, R3 = R6, R4 = R7

$$V0 = \left(1 + \frac{2R2}{R1}\right)\frac{R4}{R3}(V2 - V1)$$

Illustration is:

V0 = 101(V2 – V1)

10 Band Graphic Equalizer



202049p0

fo (Hz)	C_1	C_2	R_1	R_2
32	0.12μF	4.7μF	75kΩ	500Ω
64	0.056μF	3.3μF	68kΩ	510Ω
125	0.033μF	1.5μF	62kΩ	510Ω
250	0.015μF	0.82μF	68kΩ	470Ω
500	8200pF	0.39μF	62kΩ	470Ω
1k	3900pF	0.22μF	68kΩ	470Ω
2k	2000pF	0.1μF	68kΩ	470Ω
4k	1100pF	0.056μF	62kΩ	470Ω
8k	510pF	0.022μF	68kΩ	510Ω
16k	330pF	0.012μF	51kΩ	510Ω

Note 8: At volume of change = ±12 dB

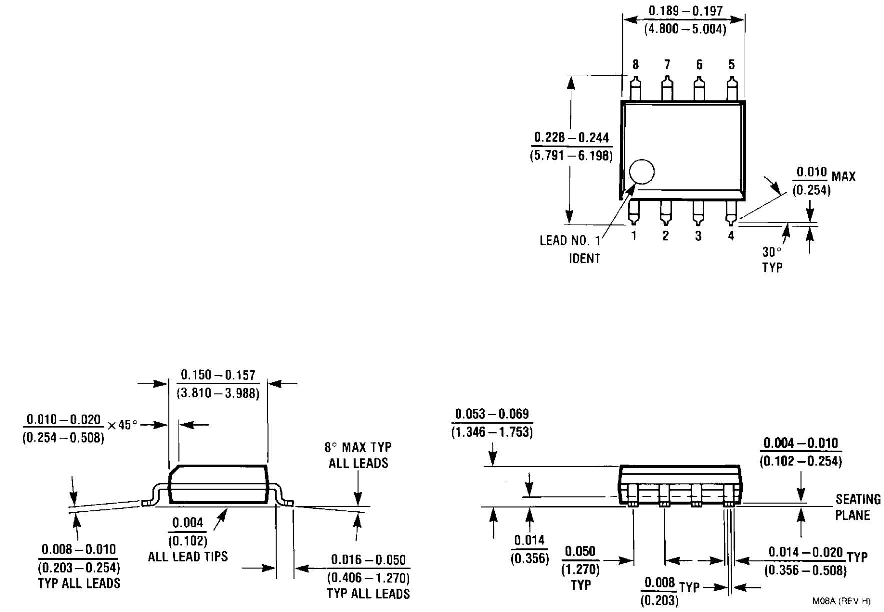
Q = 1.7

Reference: "AUDIO/RADIO HANDBOOK", National Semiconductor, 1980, Page 2–61

Revision History

Rev	Date	Description
1.0	09/26/07	Initial release.
1.1	10/01/07	Input more info under the Buffer Amplifier.

Physical Dimensions inches (millimeters) unless otherwise noted



NS Package M08A

Notes

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